# INSTRUCTION BOOK for <br> OSCILLOSCOPE OS-8C/U and OS-8E/U 

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## ORDERING PARTS

All requests or requisitions for replacement material should include the following data:

1. Standard Navy stock number or, when ordering from a Marine Corps or Signal Corps supply depot, the Signal Corps stock number.
2. Name of part and complete description.

If the appropriate stock number is not available the following shall be specified:

1. Equipment model or type designation, circuit symbol, and item number.
2. Name or part and complete description.
3. Manufacturer's designation.
4. Contractor's drawing and part number.
5. JAN or Navy type number.


Figure 1-1. Oscilloscope OS-8C/U with Cover in Place


# SECTION 1 <br> GENERAL DESCRIPTION 

## 1. PURPOSE.

This instruction book describes Oscilloscopes OS$8 \mathrm{C} / \mathrm{U}$ and $\mathrm{OS}-8 \mathrm{E} / \mathrm{U}$, and includes information concerning the operation and maintenance of the equipment. References and illustrations have been changed throughout the text only to the extent required for clarity. All reference to $\mathrm{OS}-8 \mathrm{C} / \mathrm{U}$ applies equally to $\mathrm{OS}-8 \mathrm{E} / \mathrm{U}$, except as specifically indicated.

## 2. BRIEF DESCRIPTION.

a. GENERAL.-This oscilloscope operates from 115 volts $\pm 10 \%, 50-1000$ cycles a-c, and is designed to be used as a visual testing instrument in all instances where such apparatus can be used to service electronic equipment. It has been designed to be as small and light in weight as possible, consistent with its ability to perform the functions required of it. Some of the characteristics of this oscilloscope which make it a useful instrument are: vertical a-c amplifier operating over a frequency range of 5 cycles to 2 megacycles per second, independent of gain control setting, with a sensitivity of .075 RMS volts per inch; vertical d-c amplifier operating over a frequency range of zero to 2 megacycles per second at full gain control setting; horizontal a-c amplifier operating over a frequency range of one cycle to 500,000 cycles per second, independent of gain control setting, with a sensitivity of . 075 RMS volts per inch; horizontal d-c amplifier operating over a frequency range of zero to 500,000 cycles per second at full gain control setting; selfcontained sweep circuit oscillator operating through a frequency range of 3 to 50,000 cycles per second with provisions for synchronizing of either positive or negative synchronizing voltages; provisions for beam blanking from either internal or external sources; direct access to both hor:zontal and vertical deflecting plates; shock mounted within a watertight carrying case; and of unitized construction throughout to allow for versatility and ease of servicing. In regard to this last characteristic, the oscilloscope is made up of seven major assemblies: vertical amplifier, horizontal amplifier, sweep circuit oscillator, sync. circuit, power supply, cathode ray tube assembly, and potentiometer assembly (comprised of vertical positioning, horizontal positioning, intensity and focus controls). Each of these assemblies is interchangeable from one oscilloscope to another, thus allowing for consolidation of working assemblies in case of emergency.
b. APPLICATION.--The portable construction of this oscilloscope makes it convenient to carry to any location where visual servicing is required. This oscilloscope is capable of any number of operations within its ratings, including alignment and testing of electronic and electrical equipment, hum measurements, frequency comparison, observance of complex waveforms, percentage modulation measurements, etc. Operators should familiarize themselves with each control by obtaining a pattern and then rotating the control and noting the effect, except for intensity which should not be allowed to be of extreme brilliance.

## 3. REFERENCE DATA.

a. Nomenclature: Oscilloscope $\mathrm{OS}-8 \mathrm{C} / \mathrm{U}$ or $\mathrm{OS}-8 \mathrm{E} / \mathrm{U}$, for general electronics use.
b. Contract Number: NObsr 75143 and 75682 . Date: 26 Feb. 1958 and 23 Jan. 1959.
c. Contractor: Carol Electronics Corp.
d. Cognizant Naval Inspector: Inspector of Naval Material, Baltimore, Md.
e. Number of Packages Involved per Complete Shipment of Equipment: One.
f. Total Cubical Content: Crated: $\mathbf{3 . 3 3 5} \mathbf{c u}$. in. Uncrated: $730 \mathrm{cu} . \mathrm{in}$.
g. Total Weight: Crated: 34 lbs.
Uncrated: $141 / 2 \mathrm{lbs}$.
b. Frequency Range:
(1) Vertical Amplifiers:
(a) $0-2,000,000$ cycles at full gain control setting.
(b) $5-2,000,000$ cycles, independent of gain control setting.
(2) Horizontal Amplifiers:
(a) $0.500,000$ cycles at full gain control setting.
(b) $1.500,000$ cycles, independent of gain control setting.
(3) Sweep. Circuit Oscillator: 3 to 50,000 cycles.
i. Characteristics of Power Supply Required for Operation: 105.125 volts, $50-1000$ cycles, a-c, single phase.
j. Input Impedance:
(1) Vertical: $\mathrm{AC}-1.5$ megohm shunted by 25 mmf . DC- 2 megohms.
(2) Horizontal: AC-1.5 megohm shunted by 25 mmf . DC-2 megohms
(3) Vertical Direct: 9 megohms shunted by 11 mmf .
(4) Horizontal Direct: 9 megohms shunted by 11 mmf .
k. Deflection Sensitivity:
(1) Vertical: Amplifier-. 075 RMS volts/inch. Direct-approximately 17 RMS volts/ inch.
(2) Horizontal: Amplifier- .075 RMS volts/ inch. Direct-approximately 25 RMS volts/inch.
l. Power Consumption: 60 watts at 115 volts.
m. Overall Accuracies:
(1) Vertical Amplifiers:
(a) $\pm 3 \mathrm{DB}$ from zero to $2,000,000$ cycles at full gain control setting.
(b) $\pm 3$ DB from 5 to $2,000,000$ cycles, independent of gain control setting.
(2) Horizontal Amplifiers:
(a) $\pm 3$ DB from zero to 500,000 cycles at full gain control setting.
(b) $\pm 3 \mathrm{DB}$ from one to 500,000 cycles, independent of gain control setting.

NAVSHIPS 92251
general
Paragraph 4
OS-8C/U

## 4. EGUIPMENT DATA.

TABLE 1-1. EQUIPMENT SUPPLIED

| $\begin{aligned} & \text { QUANTITY } \\ & \text { PER } \\ & \text { EQUIPMENT } \end{aligned}$ | MANE OF | NOMENClature | $\begin{aligned} & \text { OVERALL DIMENSIONS } \\ & \text { A-CRATED } \\ & \text { E-UNCRATED } \\ & \text { HEIGKT - WIDTH - DEPTM } \end{aligned}$ | $\begin{aligned} & \text { VOLUMER } \\ & \text { A-CRATED } \\ & \text { B-UNCRATED } \end{aligned}$ | $\begin{aligned} & \text { WEIGHT } \\ & \text { A-CRATED } \\ & \text { B-UNCRATED } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Oscilloscope | OS-8C/U | $\begin{gathered} \text { A: } \quad 201 / 4^{\prime \prime} \times 111 / 8^{\prime \prime} \times 143 / 4^{\prime \prime} \\ \text { B: } 9^{\prime \prime} \times 6^{\prime \prime} \times 131 / 2^{\prime \prime} \end{gathered}$ | A: $3,335 \mathrm{cu}$. in. <br> B: $\quad 730 \mathrm{cu} . \mathrm{in}$. | A: 34 lbs. <br> B: $141 / 2 \mathrm{lbs}$. |
| 1 | Case | CY-1300/U | $9^{\prime \prime} \times 6^{\prime \prime} \times 131 / 2^{\prime \prime}$ |  |  |
| 1 | Test Lead | $\begin{aligned} & 1207 / \mathrm{U} \\ & \left(3^{\prime} 0^{\prime \prime}\right) \end{aligned}$ | $3^{\prime} 0^{\prime \prime}$ |  |  |
| 1 | Test Lead | $\begin{aligned} & 1207 / \mathrm{U} \\ & \left(0^{\prime} \sigma^{\prime}\right) \end{aligned}$ | $6^{\prime \prime}$ |  |  |
| 1 | Ground Lead | W-104 | $3^{\prime} 0^{\prime \prime}$ |  |  |
| 2 | Cathode Ray Tube Screen | O-104 | 27/8" dia. |  | - |
| 2 | Instruction Book | $\begin{aligned} & \text { NAVSHIPS } \\ & 92251 \end{aligned}$ | $9^{\prime \prime} \times 111 / 2^{\prime \prime}$ |  |  |

## 5. TUBE COMPLEMENT.

TABLE 1-2. TUBE COMPLEMENT

| Tuse | TYPE | FUNCTION |
| :---: | :---: | :---: |
| V101A-V101B | 12AT7 WA | Vert. Cathode Follower-Syac. Amplifier |
| V102A-V102B | 12AT7 WA | 1st Vert. DC Amplifier |
| V103 | 6AH6 | 2nd Vert. DC Amplifier |
| V104 | 6AH6 | 2nd Vert. DC Amplifier |
| V105A-V105B | 12AT7 WA | Horiz. Cathode Follower-Intensity Modulation Amp. |
| V106A-V106B | 12AT7WA | 1st Horiz. DC Amplifier |
| V107A-V107B | 6J6WA | 2nd Horiz. DC Amplifier |
| V108A-V108B | 6J6w | Sweep Circuit Oscillator |
| V109 | 3RP1 | Cathode Ray Tube |
| V110 | 6X4W | Intermediate Voltage Rectifier |
| CR101 | Selenium | Low Voltage Rectifier |
| CR102 | Selenium | Low Voltage Rectifier |
| CR103 | Selenium | High Voltage Rectifier |

Section 2

## SECTION 2 THEORY OF OPERATION



Figure 2-1. Basic Diagram of Operation, Block Form

## 1. GENERAL.

During the following discussion, reference to the block diagram of the oscilloscope, Figure 2-1, and the schematic wiring diagram, Figure 7-11, will facilitate the understanding of the basic operation of the circuits used in this equipment.
a. VERTICAL.
(1) VERT. ATTEN. AND VERT. GAIN. (See Figure 2.2)

AC voltages applied to the vertical AC input may be attenuated by a factor of 1,10 or 100 by means of the VERT. ATTEN. control and further controlled by the position of the VERT. GAIN control. With the VERT. ATTEN. in the DC position, DC voltages may be applied to the DC input and may also be controlled by the position of the VERT. GAIN control.
(2) CATHODE FOLLOWER. (See Figure 2-3)

One-half of a type 12AT7 tube, V101A, is used as
a cathode follower to provide for high impedance vertical input circuits for AC voltages. The output voltages from this stage are taken from the low impedance cathode circuits and attenuated with a low impedance gain control before being applied to the following DC amplifier stage.
(3) AMPLIFIERS. (See Figure 2-4)

The vertical amplifiers consisting of one 12AT7, V102, and two 6AH6's, V103 and V104, connected in push-pull cascade are of the direct-coupled type and serve for amplification of both AC and DC voltages. The high frequency range of these amplifiers is 2 mc . When amplifying AC voltages, the input is condensercoupled from the cathode follower, V101A, and gives a low frequency response of 5 cycles. When serving as DC amplifiers, the input is taken directly from the VERT. GAIN control. AC voltages may be applied to the DC input for amplification by the vertical amplifiers; however, the high frequency response will be determined by the setting of the VERT. GAIN control.
b. HORIZONTAL.
(1) HOR. ATTEN. and HOR. GAIN. (See Figure 2.5)

AC voltages applied to the horizontal AC input may be attenuated by a factor of 1,10 or 100 by means of the HOR. ATTEN. control and further controlled by the position of the HOR. GAIN control. With the HOR. ATTEN. control in the DC position, DC voltages may be applied to the DC input and may also be controlled by the position of the HOR. GAIN control. With the HOR. ATTEN. control in the SWEEP position, the sawtooth output from the sweep circuit oscillator is applied to the horizontal amplifier through the horizontal cathode follower and the sweep width may be controlled by the position of the HOR. GAIN control.
(2) CATHODE FOLLOWER. (See Figure 2-6)

One-half of a type 12AT7 tube, V105A, is used as a cathode follower to provide for high impedance horizontal input circuits for AC voltages. The output voltages from this stage are taken from the low impedance cathode circuits and attenuated with a low impedance gain control before being applied to the following DC amplifier stage.

## (3) AMPLIFIERS. (See Figure 2-7)

The horizontal amplifiers consisting of a 12AT7, V106, and a 6J6, V107, connected in push-pull cascade are of the direct-coupled type and serve for the amplification of both AC and DC voltages. The high frequency range of these amplifiers is 500,000 cycles.

When amplifying AC voltages, the input is condensercoupled from the cathode follower, V105A, and gives a low frequency response of one cycle. When serving as DC amplifiers, the input is taken directly from the HOR. GAIN control. AC voltages may be applied to the DC input for amplification by the horizontal amplifiers; however, the high frequency response will be determined by the setting of the HOR. GAIN control. When the horizontal amplifiers are being used to amplify the internal sawtooth they are fed through the cathode follower, V105A, in the same manner as an external AC voltage.
c. SWEEP CIRCUIT OSCILLATOR. (See Figures 2.8 and 2-8A)

A type 6J6 tube, V108, is used in a multivibrator type circuit to generate linear sawtooth voltages for horizontal deflection of the cathode ray tube. Six positions of the COARSE FREQUENCY control are used in conjunction with a two-gang potentiometer, R158A and R158B, to provide control of sawtooth frequencies between 3 and 50,000 cycles.
d. SYNC. SELECTOR-AMPLIFIER. (See Figure 2-9)

A thrce-position SYNC. SELECTOR switch, S103, is used as a means to provide a selection of EXT., INT. or LINE frequencies to be used in connection with synchronizing the sweep circuit oscillator. Voltages selected by the SYNC. SELECTOR are fed to the control grid of one-half of the 12AT7 tube, V101B. The LOCKING control, R154, is so connected that it permits synchronization of the sweep circuit oscillator


Figure 2-2. Vertical Input Attenuator
on either positive or negative peaks of the selected synchronizing voltage.

## e. INTENSITY MODULATION AMPLIFIER. (See

 Figure 2-10)One-half of a type 12AT7 tube, V105B, is used as an amplifier whereby external or internal voltages may be amplified to provide for intensity modulation of the beam of the cathode ray tube. By connecting a jumper between BLANKING terminals on terminal board TB10s pulses from the sweep circuit oscillator may be used to blank out the return trace when using horizontal sweep.
$f$. CATHODE RAY TUBE. (See Figure 2-11)
A type 3RP1 electrostatic deflection cathode ray tube, V109, is used as the indicating medium. Deflection voltages for this tube may be applied from internal circuits, or by rearranging the jumpers on terminal board TB105 external voltages may be directly applied for deflection.

## g. POWER SUPPLY. (See Figure 2-12)

A type 6X4 tube, V110, is connected as a full-wave rectifier and supplies DC voltages for operation of the cathode followers, final amplifier stages and sweep circuit oscillator. A pair of selenium rectifiers, CR101 and CR102, are connected as a full-wave rectifier and supply low DC voltages for the operation of all the other circuits except the cathode ray tube. A selenium rectifier, CR103, is connected as a half-wave rectifier to supply the high voltage for the cathode ray tube. Suitable other windings are on the power transformer, T101, to supply the heater voltages for all tubes in the instrument. The transformer is fused by means of fuses F101 and F102 located on the front panel.

## 2. CIRCUIT ANAIYSIS.

a. VERTICAL.
(1) VERTICAL INPUT ATTENUATOR.

An AC voltage impressed between the vertical input (AC) and GND is applied through capacitor C105 to the three-stage vertical attenuator network. This network consists of resistors R102 and R103 shunted by C103 and C104 respectively, and resistor R101 shunted by C101 or C102 depending upon the position of the attenuator switch S101. The network is so designed that it is non-frequency discriminating up to square wave frequencies of 100 kc . On position " 1 " the voltage impressed is applied to grid pin 2 of the vertical cathode follower, V101A. On position " 10 " this voltage is reduced by a factor of ten, and on position " 100 " the voltage is reduced by a factor of 100 . When the VERT. ATTEN., S101, is operated to the "DC" position and a DC or AC voltage is impressed between vertical input (DC) and GND, the voltage is controlied by potentiometer R104A, the DC VERT. GAIN control, and applied to grid pin 2 of the first vertical DC amplifier, V102A.


Figure 2-3. Vertical Cathode Follower

## (2) CATHODE FOLLOWER.

One-half of a 12AT7 tube, V101A, is connected in a conventional cathode follower circuit with plate bypassed to ground by C134D and C107. Any voltage applied to the grid will, in the same phase, at a slightly lower potential, appear between the cathode and ground. Between the cathode and ground is a network composed of bias resistor R107, paralleled by C106 and AC VERT. GAIN control R104B in series. By virtue of the fact that R104B and C106 are of low impedance, the circuit capacities will be negligible and frequencies of 5 cycles to 2 mc may be controlled by R104B without frequency discrimination. The output voltage from R104B is taken through the VERT. ATTEN. switch, S101, and applied to the grid, pin 2 of the first vertical DC amplifier, V102A.

## (3) VERTICAL AMPLIFIERS.

The vertical amplifiers are of the direct-coupled push-pull type. This allows the amplification of DC as well as AC voltages. The fact that the amplifiers are push-pull affords excellent stability with line voltage variations.

When amplifying AC voltages, the signal is applied to grid pin 2 of V102A from the center arm of the low impedance gain control, R104B, through switch S101. The resistance of R104B is low enough so as to afford no frequency discrimination and therefore the position of the gain control has no effect on the band width when in the "A.C." attenuator positions. When amplifying DC voltages, the signal is applied


REFER TO OVERALL SCHEMATIC DRAWING.

Figure 2-4. Vertical Amplifiers
to grid pin 2 of V102A from the center arm of the high impedance gain control, R104A, through switch S101. The resistance of R104A is high and therefore when the attenuator is in the "D.C." position the gain control acts as a frequency sensitive voltage divider varying the band width as in Table 2-1. When the
table 2-1. Effect of Vertical Gain Control Setting on Bandwidth for Vertical "D.C." Input.

| Gain Control Setting | Approximate Band Width |
| :---: | :---: |
| 100 | $2,000,000 \mathrm{cps}$ |
| 75 | $300,000 \mathrm{cps}$ |
| 50 | $2,000,000 \mathrm{cps}$ |
| 25 | $3,000,000 \mathrm{cps}$ |

VERT. ATTEN., S101, is on the "D.C." position, there is a slight negative contact potential developed on grid pin 2 because of the high impedance in that circuit. This voltage is cancelled out by a B+ voltage applied through R109. The bias for V102A is supplied by cathode resistor R110. When amplifying AC voltages the cathode is bypassed through C108 to eliminate degeneration; however, when amplifying DC voltages this cathode is left unbypassed to eliminate low frequency discrimination. The B+ voltage is supplied to the plate of this amplifier through plate load resistor R116 which is balanced with plate load resistor R117 of the other portion (V102B) of the first push-pull amplifier. Grid pin 7 of V102B is held at a low impedance to ground through R113. This grid carries no
signal except at high frequencies as will be explained later. The bias for V102B is supplied by the cathode resistance of the VERT. POS. control, Ril1.

The output from this first push-pull amplifier is applied between the grids, pins 1 of V103 and V104, which comprise the second push-pull amplifier, through resistors R115 and R118. These resistors act to suppress any tendency for spurious oscillation. The cathodes of V103 and V104 are tied together and biased to ground through resistor R120, R190 and BIAS ADJUST, R119. Since the grids of V103 and V104 are approximately 80 volts above ground, because of the direct connection from the previous stage, the cathode must develop a voltage slightly higher than this to supply sufficient operating bias. The B+ voltage is supplied to the plates, pins 5 of V103 and V104, through plate load resistors R123 and R124. The screen grids, pins 6 of V103 and 104, are tied together and supplied with voltage through a common screen dropping resistor, R122, shunted by LINEARITY control, R121. Since these tubes are operating in push-pull, there is no need for bypass on these screens. The suppressor grids, pins 2 of V103 and V104, are tied to the cathode as in normal pentode connection when the cathode is operated above ground. The signal is directly coupled from the plates, pin 5, of the final push-pull amplifier stage, to the deflection plates of the cathode ray tube through terminal board TB105.

Since the circuit is designed in push-pull, any B+ variation caused by fluctuating line voltages has essentially no effect on the centering of the beam of
the cathode ray tube, as a voltage change on one plate is accompanied by an equal voltage change on the other plate. The path of the signal is through one side of the first push-pull amplifier, V102A, and on to the grid, pin 1, of V103. It is then transferred to V104 through the common cathode resistance R120, R190 and BIAS ADJUST R119 in series. The action is as follows. As a positive signal appears on grid pin 1 of V103 this tube draws more current. As the current increases the voltage at cathode pin 7 will rise. This rise is carried to cathode pin 7 of V104 by virtue of the common cathode connection. Since grid pin 1 of V10. ${ }^{\text {is at a }}$ a stationary potential as far as the signal is concerned, the rising cathode voltage causes this tube to draw less current, accomplishing a push-pull double-ended output between the plates, pins 5 , of V103 and V10́t.
At high frequencies a portion of the signal on the plate of V102A is fed to grid pin 7 of V102B through trimmer condenser C109. This high frequency signal is transferred from the plate of V102B to the grid of V10f and boosts the high frequency output. Trimmer condenser C 109 is adjusted to give the amplifier sufficiently high frequency response. Resistors R189 and R111 together form a voltage dividing network that balances both triodes of V102 for proper vertical centering. BIAS ADJUST R119 is provided so that tolerances in resistors and electron tubes may be accounted for in providing the proper bias on the final stage. A LINEARITY adjustment, R121, is incorporated in the circuit to adjust the voltage on the screens of the final push-pull stage (V103 and V104) in order to accomplish maximum linearity with changes in
tubes. Normally, these controls will not have to be adjusted unless tubes V102, V103 and V104 are changed, in which case the adjustments will be minor.

## b. HORIZONTAL.

(1) HORIZONTAL INPUT ATTENUATOR.

An AC voltage impressed between the horizontal input (AC) and GND is applied through capacitor C110 to the three-stage horizontal attenuator network. This network consists of resistors R126 and R127 shunted by C114 and C115 respectively, and resistor R128 shunted by C111 or C112 depending upon the position of the attenuator switch S102. The network is so designed that it is non-frequency discriminating up to the square wave frequency of 25 kc . On position " 1 " the voltage impressed is applied directly to grid pin 2 of the horizontal cathode follower, V105A. On position " 10 " this voltage is reduced by a factor of ten, and on position " $100^{\text {" the voltage is reduced by }}$ a factor of 100. When the HOR. ATTEN., S102, is operated to the "DC" position and a DC or AC voltage is impressed between the horizontal input (DC) and GND, the voltage is controlled by potentiometer R129A, the DC HOR. GAIN control, and applied to grid pin 2 of the first horizontal DC amplifier, V106A. When the HOR. ATTEN., S102, is operated to the "SWEEP" position the internal sawtooth voltage is fed to grid pin 2 of the horizontal cathode follower, V105A, shunted by the resistor-capacitor combination R125 and C113.
(2) HORIZONTAL CATHODE FOLLOWER.

One-half of a 12AT7 tube, V105A, is connected in the conventional cathode follower circuit with plate


Figure 2-5. Horizontal Input Attenuator


Figure 2-6. Horizontal Cathode Follower
bypassed to ground by C13.4C and C117. Any voltage applied to the grid will, in the same phase, at a slightly lower potential, appear between the cathode and ground. Between the cathode and ground is a network composed of bias resistor R132, paralleled by

Cll6, and the AC HOR. GAIN control, R129B, in series. By virtue of the fact that R129B and C116 are of low impedance, the circuit capacities will be neg. ligible and frequencies of one cycle to 500 kc may be controlled by R129B without frequency discrimination. The output voltage of R129B is taken through the HOR. ATTEN., S102, and applied to grid pin ? of the first horizontal DC amplifier, V106A.

## (3) HORIZONTAL AMPLIFIERS.

The horizontal amplifiers are of the direct-coupled push-pull type. This allows the amplification of DC as well as AC voltages. The fact that the amplifiers are push-pull affords excellent stability with line voltage variations. When amplifying AC voltages or the internal sawtooth, the signal is applied to grid pin 2 of V1OGA from the center arm of the low impedance gain control, R129B, through switch S 102. When amplifying DC voltages, the signal is applied to grid pin 2 of V10GA from the center arm of the high impedance gain control, R129A, through S102. When HOR. ATTEN., S102, is on the "DC" position, there is a slight negative contact potential developed on grid pin 2 of V10GA because of the high impedance in that circuit. This voltage is cancelled out by a B voltage through R133. The bias for V106A is supplied by cathode resistor R13.f. When amplifying AC voltages the cathode is bypassed through C118 to climinate degeneration; however, when amplifying DC. voltages this cathode is left unbypassed to eliminate low frequency discrimination. The B+ voltage is supplied to the plate of this amplifier through plate load resistor R139 which is balanced with plate load resistor


Figure 2-7. Horizontal Amplifiers

R140 of the other portion (V106B) of the first pushpull amplifier. Grid pin 7 of V106B is held at a low impedance to ground through R138. This grid carries no signal except at high frequencies as will be explained later. The bias for V106B is supplied by the cathode resistance of the HOR. POS. control, R136.

The output from this first push-pull amplifier is - applied between the grids, pins 5 and 6 of V107, which comprises the second push-pull amplifier, through resistors R143 and R144. These resistors act to suppress any tendency for spurious oscillation. The cathode of V107 is biased to ground through resistor R142 and BIAS ADJUST, R141. Since the grids of V107 are approximately 60 volts above ground, because of the direct connection from the previous stage, the cathode must develop a voltage slightly higher than this to supply sufficient operating bias. The B + voltage is supplied to the plates, pins 1 and 2 of V107, through piate load resistors R145 and R146. The signal is directly coupled from these to the deflection plates of the cathode ray tube through terminal board TB105.

Since the circuit is designed in push-pull, any $\mathbf{B}+$ variation caused by fluctuating line voltage has essentially no effect on the center of the beam of the cathode
ray tube, as a voltage change on one plate is accompanied by an equal voltage change on the other plate. The path of the signal is through one side of the first push-pull amplifier, V106A, and on to the grid, pin 6 of V107A. It is then transferred to V107B through the common cathode resistance R142 and BIAS ADJUST R141 in series. The action is as follows: As a positive signal appears on grid pin 6 of V107A this tube draws more current. As the current increases the voltage at cathode pin 7 will rise. Since grid pin 5 of V107B is at a stationary potential as far as the signal is concerned, the rising cathode voltage causes V107B to draw less current, accomplishing a push-pull double-ended output between the plates, pins 1 and 2 , of V107

At high frequencies a portion of the signal on the plate of V106A is fed to grid pin 7 of V106B through trimmer condenser C119. This high frequency signal is transferred from the plate of V106B to the grid of V107B and boosts the high frequency output. Trimmer condenser C119 is adjusted to give the amplitier ${ }^{-}$ sufficiently high frequency response. Resistors R187 and R138 together form a voltage dividing network that balances both triodes of V102 for proper horizon-


Figure 2-8. Sweep Circuit Oscillator

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tal centering. BIAS ADJUST R141 is provided so that tolerances in resistors and electron tubes may be accounted for in providing the proper bias on the final stage. Normally, these controls will not have to be adjusted unless tubes V106 and V107 are changed, in which case the adjustments will be minor.

## c. SWEEP CIRCUIT OSCILLATOR.

A cathode coupled, multivibrator circuit utilizing a type 6 J 6 tube, V108, is used as the horizontal sawtooth oscillator and operated over a frequency range from 3 to 50,000 cycles per second. This range of frequencies is controlled by the COARSE FREQUENCY switch, S104, utilizing capacitors C125 through C131. These capacitors act alternately and respectively as sawtooth generating capacitors for the second triode section, V108B, and as coupling capacitors for the first triode section, V108A, to the second triode section of the multivibrator. In the position shown in Figure 2-8, C125 is used as a sawtooth capacitor while C126 is the coupling capacitor.

Fine frequency control is accomplished by means of the dual VERNIER FREQUENCY potentiometer, R158A and R158B, in the plate circuit and in the grid of the second triode section of the multivibrator. Both potentiometers are on the same shaft and operated by the VERNIER FREQUENCY control on the SWEEP CIRCUIT OSCILLATOR panel.

The sawtooth output is taken from plate pin 1 of


Figure 2-8A. Sweep Circuit Oscillator, Simplifed

V108B through the frequency compensated voltage divider consisting of R155 shunted by C123 (Fig. 2-8) and R125 shunted by C113 (Fig. 2-5), and decoupled by capacitor C124. This sawtooth signal is applied to the horizontal cathode follower through HOR. ATTEN. S102 when set to the "SWEEP"' position. The high frequency linearity of the sawtooth may be adjusted with capacitor C123 in the frequency compensated dividing network.

Bias for the multivibrator is supplied by cathode resistor R161. The wave form at the cathode consists of sharp pulses of the exact width of the retrace time and in the proper phase. These pulses may be jumpered at terminal board TB10S to the input of the intensity modulation amplifier and thus provide return trace elimination when using the sweep circuit oscillator. The synchronizing signal from the LOCKING control, R154, is applied to grid pin 5 of V108A through isolation resistor R162. This causes the frequency of the multivibrator to lock in at the frequency of the synchronizing signal or some submultiple thereof.

## d. SYNC. SELECTOR-AMPLIFIER.

The purpose of the SYNC. SELECTOR switch, S103, and amplifier is to provide a means of synchronizing the sweep circuit oscillator from either


Figure 2-9. Sync. Selector-Amplifior

EXT., INT. or LINE frequency voltages and to permit the synchronization of the sweep circuit oscillator from either positive or negative peaks of the applied synchronizing voltage. The output from the SYNC. SELECTOR is fed through capacitor C121 to grid pin 7 of V101B and selects either:
(1) line frequency voltage supplied from the filament winding through a voltage divider consisting of R149 and R148,
(2) external frequency voltage applied to binding post E108, or
(3) internal frequency voltage supplied from the low impedance cathode of the 2nd vertical d-c amplifier (V103 and V10.4), through decoupling resistor, R108. The grid of the sync. amplifier, V101.B, is returned to the junction of R153 and R152 through resistor R151 to provide sufficient bias for operation of the amplifier.

An analysis of the circuits between the plate of V101B and ground will show that with a signal applied to the control grid, the high end of the LOCKING control, R154, will be electrically receiving signals developed at the plate of this tube; and the low end of the LOCKING control will be receiving signals from the cathode. When this control is at approximately the center of its rotation there is no signal since the center of the control is grounded. If this control is operated toward the plate side of R154 a locking voltage would be obtained which would be out of phase with the signal applied to the grid and consequently, tend to lock the sweep circuit oscillator at a polarity with respect to the negative peaks of the synchronizing signal. If the LOCKING control is advanced toward the cathode side of R154 the locking voltage applied to the sweep circuit oscillator would be in positive phase relation to the synchro-


Figure 2-10. Intensity Modulation Amplifier
nizing signal. As a result of this circuit, the sweep circuit oscillator may be locked in with respect to incoming synchronizing signals, either in phase or out of phase with these voltages.

## c. INTENSITY MODULATION AMPLIFIER.

In cathode ray oscilloscope nomenclature a modulation of the intensity of the cathode ray tube beam is known as Z AXIS modulation. Such modulation is often useful to establish a time base for the horizontai deflection of the cathode ray tube beam. As an example, the beam might be modulated by a 1000 cycle source which would cause it to increase in brilliance and decrease each one-thousandth of a second. or each one-thousand microseconds. With this intensity modulation superimposed upon an observed wave form its duration could be calculated.

One-half of a type 12 AT '7 tube, V105B, is utilized as an amplifier to provide intensity modulation for the cathode ray tube beam. Voltages to actuate this amplifier may be taken from the Z AXIS input, or by means of a jumper on the rear terminal boardTB105, pulses may be taken from the sweep circuit oscillator to provide beam banking during the return trace when using the sweep circuit oscillator for horizontal deflection. If the voltage is taken from the Z AXIS input it is applied to grid pin 7 of V105B through capacitor $\mathrm{Cl20}$. However, if the pulses from the sweep circuit oscillator are used for internal beam blanking the signal is directly coupled to the grid from the cathode of the sweep circuit oscillator to eliminate low frequency discrimination. Resistor R164 acts as a grid return to ground. Bias for this amplifier is provided in the cathode circuit by resistor R166 shunted by capacitor C132. This resistor-capacitor combination provides compensation for improving the high frequency response of this amplifier. The $\mathrm{B}+$ is supplied to the plate through resistor R165 and the output is taken from the plate through capacitor C136 and applied directly to the control grid of the cathode ray tube, V10). Positive voltages applied to the $Z$ AXIS input will cause blanking action of the cathode ray tube beam.

## $f$. CATHODE RAY TUBE.

A type 3RP1 cathode ray tube, V109, is used as the indicating medium in the oscilloscope. This tube utilizes electrostatic deflection and has four free deflecting plates. Voltage for the operation of this tube is obtained from the high voltage section of the power supply, the negative side of which is filtered and applied through R179 to the control grid, pin 2 of V109. Intensity (INT.) control, R176, is connected directly from the negative side of the high voltage power supply to R177, the FOCUS control. Cathode pin 3 of V109 is connected to the center arm of INTENSITY control R176 through resistor R180. As the INT. control is operated, it varies the potential difference between the cathode of V109 and the control grid, thereby controlling the intensity of the beam. FOCUS control, R177, is returned to ground through R178 and serves to focus the cathode ray tube beam. Anode \#2 and grid \#2, pin 8 of V109, are supplied with B+ NAVSHIPS 92251 OS-8C/U

THEORY OF


Figure 2-11. Cathode Ray Tube
through the voltage divider consisting of resistors R181 and R182. The voltage at the output of this divider determines the astigmatic focus and is designed to be equal to the nominal DC voltage of the deflection plates, pins 6, 7, 9, and 10 of V109.

The vertical and horizontal deflection plates, pins $6,7,9$ and 10 respectively, are directly connected to terminal board TBios. When the jumpers on this terminal board are arranged for internal connection the output leads from the vertical and horizontal amplifiers are connected directly to the deflection plates. When the jumpers are arranged for external connection, the output leads from the vertical and horizontal amplifiers are connected to the deflection plates through resistors R183 to R186 inclusive. These resistors provide the DC voltage and centering that was present with the internal connection; however, no signal is carried to the deflection plates. With this connection, an external signal may be applied to the deflection plates through capacitors C137 to C140 inclusive by connecting the external signal to the terminals marked EXT. INPUT. If it is desired to use an external capacitor to couple the signal directly to the deflection plates, this capacitor may be connected to the terminals marked D1 through D4 on the terminal board TB105.

## g. POWER SUPPLY.

All voltages for operation of the oscilloscope are obtained from the power supply utilizing transformer T101. The primary of this transformer is connected to the permanent AC power cable W103. Fuses F101 and F102 are used between the input and the primary. The POWER OFF-ON switch, S105, is connected in series with one fuse and one side of the primary. There are basically four secondary windings on the transformer. One of these is center-tapped to ground and provides two full-wave voltages, approximately 90 and .325 volts, on each side of the center tap. The 325 volt winding is connected to the plates, pins 1 and 6 , of the intermediate voltage rectifier, V110. The output is taken from cathode pin 7 of this rectifier and suitably filtered by mearrs of capacitors C135A and C135B in conjunction with resistor R171 to provide B + voltage for the final stages of the horizontal amplifier. This output is also decoupled by means of resistors R172 and R173 and capacitor C135C, and acts to supply the $B+$ voltage for the final stages of the vertical amplifiers. The $B+$ voltages for the vertical and horizontal cathode followers are provided by the decoupling networks consisting of R175 and C134D, and R174 and C134C respectively.


Figure 2-12. Power Supply

The 90 volt winding is connected to the plates of CR101 and CR102 through protective resistors R167 and R168. The output from these selenium rectifiers is filtered by C134A and C134B in conjunction with R170 to provide low voltage B+ supply for the first push-pull horizontal and vertical amplifier stages.

Another secondary winding has its low voltage side tied to one side of the 325 volt winding and its high voltage side tied to the cathode of selenium rectifier

CR103. The output from this rectifier is filtered by C133A and C133B in conjunction with R169 and provides a high negative voltage for operation of the cathode ray tube.

A separate 6.3 volt winding is used to supply the heater of the cathode ray tube, V109. Another 6.3 volt winding, center-tapped to ground, is used to supply the heaters of all other tubes in the equipment.

GENERAL DESCRIPTION


Figure 3-1. Overall Outline Dimensions of Oscilloscope OS-8C/U


Figure 3-2. Cutaway View of Export Packaging

## SECTION 3

## INSTALLATION AND INITIAL ADJUSTMENT

## 1. INSTALLATION.

a. HOUSING.-Oscilloscope OS-8C/U, together with all accessories except the instruction book, is housed in a water-tight metal case consisting of a bottom section in which the unit is secured by four shock mounts, and an upper cover which is secured to the lower case by four drawbolts. The upper cover is sealed to the lower case by means of a rubber gasket making the instrument water-tight when the upper cover is in place.

A compartment is provided in the right side panel of the main unit for storing the line cord (See Figure 3-4). The test leads are stored in the front corner of the case.
b. UNPACKING.-When opening the packing case and removing the equipment (See Figure 3-2), care should be taken not to dent or otherwise damage the metal housing of the equipment in order to preserve its water-tightness.
c. OPERATING LOCATION.-In general, with very few exceptions, any location where suitable AC input power is available will be a satisfactory operating location for the equipment. However, it should NOT be operated adjacent to or in the vicinity or large electrical generating equipment or in close
proximity to other apparatus which might be generating large stray magnetic fields, as this will tend to distort the patterns displayed on the screen of the cathode ray tube.

## Note

The equipment has been designed to operate equally well in any convenient operating position.

## d. OPERATING CABLES.

(1) AC LINE CORD.-A 5-foot AC line cord (W103) will be found in the accessory compartment on the right side of each equipment. This cord is permanently connected to the oscilloscope on one end and is fitted on the other end with a standard 2-prong male AC line plug. The shield of the power cord is terminated in a lug suitable for retention by an 8.32 roundhead machine screw on the end having the $\mathbf{2}$-prong male plug.
(2) TEST CABLES.-Supplied as accessories to each equipment are one 36 -inch shielded coaxial cable (W101) and one 6 -inch shielded coaxial cable (W102) for use in connection with the vertical input circuits. A 3-foot unshielded test lead (W104) is supplied to be used for connection between the chassis of the $\mathrm{OS}-8 \mathrm{C} / \mathrm{U}$ or $\mathrm{OS}-8 \mathrm{E} / \mathrm{U}$ oscilloscope and ground side of the voltage to be observed.


Figure 3-3. Oscilloscope OS-8 C/U Front Oblique View


Figure 3-4. Oscilloscope OS8-C/U Right Cable Compartment and Terminal Board, Rear Oblique View

AND ADJUSTMENT

## 2. ADJUSTMENT.

## WARNING

THE VOLTAGES WHICH ARE UTILIZED IN THIS EQUIPMENT ARE DANGEROUS TO HUMAN LIFE. BEFORE REMOVING THE EQUIPMENT FROM ITS CASE FOR INSPECTION, THE AC LINE PLUG WHICH FITS INTO THE POWER RECEPTACLE SHOULD BE COMPLETELY REMOVED. SHOULD IT BE NECESSARY TO TAKE VOLTAGE READINGS WITHIN THE INSTRUMENT, MAKE SURE HANDS ARE DRY, USE TEST PRODS INSULATED FOR AT LEAST 2500 VOLTS, AND IN ALL POSSIBLE CASES MAKE ALL READINGS AND ADJUSTMENTS WITH ONE HAND IN A POCKET.
a. INSPECTION.-Before applying AC power to this equipment for the first time; inspect the entire equipment as follows:
(1) Make certain that there are three test leads in addition to the AC line cord in the accessory compartments, and check carefully for mechanical damage to connectors or cables.
(2) Loosen the six screws securing each side panel to the main unit and inspect chassis to make certain that all tubes are undamaged and in their proper sockets.
(3) Give the entire equipment a careful mechanical inspection to make certain there are no damaged components.
(4) Replace side panels.
b. TESTS PRECEDING OPERATION.-The following measurements should be made prior to placing the equipment in operation:
(1) With a continuity tester, check the test cables for open or short circuits.
(2) With the AC line cord disconnected from the power supply, but with the INT. control rotated a sufficient distance to place the AC line switch in the "ON" position, check with an ohmmeter the DC resistance between the two prongs of the male AC line plug. This resistance should be about 8 ohms. If it should vary substantially from this value, or show no continuity at all, inspect fuses, AC line switch on the INT. control, and all wiring, for cause of trouble.
c. INITIATING OPERATION.-With the AC line cord inserted into any convenient source of 115 volts $\pm 10 \%$, 50 to 1000 cycles AC , the equipment is set in operation by rotating the INT. control in a clockwise direction away from the position marked "OFF". Operation will be indicated by the glow of the pilot light E109 near the bottom of the front panel. Within approximately one minute, the beam should appear on the cathode ray tube screen.
d. CHECKING OPERATION.-Check operation of the positioning (POS.), FOCUS and intensity (INT.) controls. By turning the COARSE FREQUENCY switch through all positions, with the HOR. ATTEN. switch in the "SWEEP" position and advancing the HOR. GAIN control, proper operation of the sweep circuit oscillator will be indicated by horizontal deflection of the beam.

## Note

In order to prevent burning the screen of the cathode ray tube, always set the INT. control at the point which will give a trace no brighter than that which can be conveniently seen with the light shield extended.

## 1. FUNCTION OF EQUIPMENT.

Since Oscilloscope OS-8C/U is operated in a conventional manner, only a basic knowledge of cathode ray oscilloscopes is required for its application and operation. Therefore, this section will be concerned with the specific controls of the equipment and their functions.

## 2. CONTROLS AND THEIR FUNCTIONS.

The front panel views illustrated in Figures 4-1 and 4.2 show the location of all operating controls.
a. INT.-OFF (R176, S105).-Operating the intensity control clockwise turns the power on to the instrument and the pilot light E109 will indicate that the instrument is on. As this control is operated further clockwise, it controls the intensity of the pattern on the cathode ray tube. When moved to full clockwise position, the pattern is at maximum brilliancy.
b. FOCUS (R177).-This control adjusts the focus, or sharpness, of the trace on the screen of the cathode ray tube.
c. POS. (LEFT-RIGHT (R136), DOWN-UP (R111)).-The purpose of the positioning controls is to adjust the position of the trace on the screen, either horizontally or vertically.
d. VERT. ATTEN. (S101).

## Important Note

Always operate the VERT. ATTEN. switch to the highest attenuator position in which suitable vertical deflection can be obtained. If this is not done, overloading of the cathode follower will generally result. Overloading can be detected by a clipping or squashing of the pattern.
This control attenuates the signal fed in at the vertical input (AC) connector by a factor of 1,10 or 100. When turned to the " DC " position, it permits the DC voltages fed in between the DC input and GND to be amplified by the vertical amplifier. Positive DC voltages will cause the beam to move up on the screen.
e. VERT. GAIN (R104).-This control is used as a vernier in connection with the VERT. ATTEN. to control the height of the pattern on the screen in the case of AC voltages; and in the case of DC voltages, the extent of deflection, either up or down, of the beam. The position of the gain control has no effect on band width when the attenuator is in the "AC" positions; however, in the "DC" position the gain control affects the band width as indicated in Table 2-1.
$f$. HOR. ATTEN. (S102).

$$
\begin{aligned}
& \text { Important Note } \\
& \text { Always operate the HOR. ATTEN. switch to } \\
& \text { the highest attenuator position in which suit- } \\
& \text { able horizontal deflection can be obtained. If } \\
& \text { this is not done, overloading of the cathode } \\
& \text { follower will generally result. Overloading }
\end{aligned}
$$

can be detected by a clipping or squashing of the pattern.
This control attenuates the signal fed in at the horizontal input (AC) connector by a factor of 1,10 and 100. When turned to the "DC" position, it permits the DC voltages fed in between the DC input and GND to be amplified by the horizontal amplifier. Positive DC voltages will cause the beam to move to the right on the screen. This control, when turned to the "SW'EEP" position, permits the sawtooth from the sweep circuit oscillator to be amplified by the horizontal amplifier, thus providing horizontal deflection.
g. HOR. GAIN (R129).-This control is used as a vernier in connection with the HOR. ATTEN. to control the width of the pattern on the screen in the case of external AC voltages; and in the case of DC voltages, the extent of deflection, either left or right, of the beam. When the HOR. ATTEN. is in the "SWEEP" position, the HOR. GAIN controls the width of the sweep.
b. COARSE FREQUENCY (S104).-This control selects the range of frequencies of the internal sweep circuit oscillator which may operate between the limits of 3 and 50,000 cycles. Although the frequency ranges are marked on the panel for convenience of the operator, these frequencies are only approximate and, in general, the actual frequency range will be much greater so that two consecutive frequency ranges will exhibit a sizeable overlap.
i. VERNIER-FREQUENCY (R158).-This control serves as a vernier on the frequency being generated by the sweep circuit oscillator in any one of the six positions of the COARSE FREQUENCY control.
j. SYNC. SELECTOR (S103).-This control selects synchronizing voltage for application to the sweep circuit oscillator. These synchronizing voltages may be selected either from an external source, internal source which is the voltages being applied to the vertical amplifiers, or from an internal source of line frequency voltage.
k. LOCKING (R154).-This control permits selection of either positive or negative peaks of synchronizing voltages and, in addition, controls the extent of locking voltage applied to the sweep circuit oscillator.

## l. TERMINALS.

VERTICAL INPUT (AC) (J101).-lnput for AC voltages deflecting the beam vertically on the cathode ray tube screen.

VERTICAL INPUT (DC) (E102).-Input for DC voltages applied to the vertical amplifiers.

HORIZONTAL INPUT (AC) (E103).-Input for AC voltages deflecting the beam horizontally on the cathode ray tube screen.



Figure 4-2. Panel Connectors and Controls, Top View

HORIZONTAL INPUT (DC) (E105).-Input for DC voltages applied to the horizontal amplifiers.

GND (2) (E101, E104).-Direct connection to chassis of equipment and to one side of all other externally applied voltages.

EXT. (E108).-Input for external synchronizing voltages to be used in synchronizing the sweep circuit oscillator.

LINE (E106).-A source of line supply frequency to be used either in causing deflection for horizontal or vertical inputs, or as a source of line frequency for any other use to which it might be put.

Z AXIS (E107).-Connection for an external voltage to be used in intensity modulating the cathode ray tube beam.

TERMINAL BOARD (TB105)-Permits direct connection to either horizontal or vertical deflection plates and provides means of beam blanking from internal sweep circuit oscillator.


Figure 4-3. Rear Terminal Board TB105

## 3. OPERATION.

a. OBSERVING WAVE FORMS USING INTERNAL SWEEP AND SYNC.

Connect the source of alternating voltage to be observed to the vertical input (AC) and GND connections. Set the COARSE FREQUENCY control, S104, to the slowest sweep frequency, position "3-18". The SYNC. SELECTOR, S103, should be turned to "INT", while the LOCKING control, R154, is turned to the zero position. Adjust VERT. GAIN R104 and VERT. ATTEN. S101 for suitable vertical deflection. Adjust HOR. GAIN R129 until the pattern is of the desired width. W'hen the pattern first appears it will usually show many cycles as the picture of the sine wave under observation in Figure $\mathbf{4}-\mathbf{4}$. Slowly rotate the VERNIERFREQUENCY, R158, until the number of cycles decreases to the desired number. If the number is still greater than convenient, then COARSE FREQUENCY S104 should be rotated to the next clockwise position and fewer cycles will appear as shown in Figure 4-5. When the desired number of cycles are obtained, the trace can be locked in by rotating the LOCKING control, R154, either clockwise or counter-clockwise, depending upon whether it is desired to lock in positive or negative synchronizing pulses.
b. OBSERVING WAVE FORMS USING INTERNAL SWEEP AND EXT. SYNC.

Follow all steps outlined in paragraph 3(a) with the following exception:

SYNC. SELECTOR S103 is turned to "EXT" rather than "INT", and the source of synchronizing voltage is applied between the EXT. binding post and GND.
c. OBSERVING WAVE FORMS USING INTER. NAL SWEEP WITH LINE FREQUENCY SYN. CHRONIZING VOLTAGES.

Follow all steps outlined in paragraph 3(a) with the following exception:

When the sweep circuit is to be locked in at line frequency, SYNC. SELECTOR S103 is turned to "LINE".
d. OBSERVING WAVE FORMS USING INTERNAL SINE WAVE LINE FREQUENCY SWEEP.

Connect the source of alternating voltage to be observed between the vertical input (AC) and GND. Set the HOR. ATTEN., S102, to the AC divided by 10 position. Make an electrical connection between the LINE binding post and the horizontal input (AC) binding post. Operate the HOR. GAIN and VERT. GAIN controls to give the desired size of pattern. LOCKING, VERNIER-FREQUENCY and SYNC.. SELECTOR controls have no effect upon the operation.
e. OBSERVING PATTERNS WITH SINE WAVE VOLTAGES IN BOTH HORIZONTAL AND VER. TICAL INPUTS.

Connect the two voltages for comparison to the oscilloscope, one on the horizontal input (AC) and one on the vertical input (AC). Adjust the HOR. ATTEN., S102, and VERT. ATTEN., S101, to the highest attenuation position that will give suitable deflection in both directions. Adjust the HOR. GAIN and VERT. GAIN controls until the pattern is of the desired size. With the above controls so adjusted, as the two frequencies become exact ratios of one another definite patterns, as illustrated in Figures 4-6 and 4-7, will appear on the screen.

The rule for determining ratios is to count the number of times the pattern touches one axis and then the number of times it touches the other. The ratio between the two is the ratio of the two frequencies. If the beam touches the horizontal axis more often than the vertical axis, then the beam must be moving more slowly in the horizontal direction than it is in the vertical direction. This being the case, the slowest frequency is being fed into the horizontal amplifier.

## $f$. VERTICAL DEFLECTION WITH DC INPUT.

Operate the VERT. ATTEN., S101, to the "DC" position. Apply DC voltage to the (DC) vertical input connection, E102, and adjust VERT. GAIN R104 to give the desired deflection sensitivity.
g. HORIZONTAL DEFLECTION WITH DC INPUT.

Operate HOR. ATTEN. S102 to the "DC" position. Apply. DC voltages to the (DC) horizontal input con-
nection. E105, and adjust HOR. GAIN R129 to give the desired deflection sensitivity.
b. APPLYING VOLTAGE DIRECTLY TO DEFLECTION PLATES. (See Figure 4-3)

## WARNING

The voltages that appear on the bottom two rows of terminals on TERMINAL BOARD TB105 are by necessity high and dangerous to human life. Before changing any jumper connections on these terminals, de-energize the oscilloscope.


Figure 4-3A-Rear Terminal Board TB105 showing the addition of larger external capacitors.
(1) VERTICAL PLATES.-To apply voltages directly to the vertical deflection plates, change the jumpers on the vertical side of the board from "INT" to "EXT" connection as indicated by the dotted lines on the diagram appearing on the cover of TERMINAL BOARDTB105: The deflecting voltages may then be applied to the two terminals marked "EXT. INPUT". These terminals are isolated from the voltage on the deflection plates through capacitors C137 and C138. In observing very low frequency wave forms, the time constant of this input circuit may become objectionable. In this case, larger external capacitors may be connected between the terminals marked "EXT. INPUT" and the terminals marked D3 and D4 (See Figure 4.3A).
(2) HORIZONTAL PLATES.-To apply voltages directly to the horizontal deflection plates, change the jumpers on the horizontal side of the board from "INT" to "EXT" connection as indicated by the dotted lines on the diagram appearing on the cover of TERMINAL BOARDTB105. The deflecting voltages may then be applied to the two terminals marked "EXT. INPUT". These terminals are isolated from the voltage on the deflection plates through capacitors C139 and C140. In observing very low frequency wave forms, the time constant of this input circuit may become objectionable. In this case larger external capacitors may be connected between the terminals marked "EXT. INPUT" and the terminals marked D1 and D2 (See Figure 4-3A).

## i. RETURN TRACE ELIMINATION. (See Figure

 4-3)When using the sweep circuit oscillator for horizontal deflection, should it be desired to blank the beam out on the return trace, a jumper should be installed between the two INTERNAL BLANKING terminals on the TERMINAL BOARD TB105. With these terminals connected together voltage should not
be fed in at the Z AXIS binding post, E107, on the main panel to avoid distorting the saw tooth output of the sweep circuit oscillator.
j. OTHER APPLICATIONS OF THE OSCILLO. SCOPE.

In addition to using the OS-8C/U for observation of wave forms as outlined in paragraphs 3(a) through 3(i), the oscilloscope may find use in many other applications such as:
(1) Alignment of tuned R.F. and I.F. stages and video circuits,
(2) Alignment of F.M. discriminator stages,
(3) Observation of irregular wave shapes, pulses, etc.,
(4) Approximate measurements of percent distortion,
(5) Detection and identification of hum in power supplies, and
(6) Determination of percent modulation in transmitters.
(7) Due to the wide frequency response of the vertical amplifiers, being from zero cycles on DC to $2 \mathrm{mc} A C$, the instrument will find extremely wide uses in connection with measurements and observation of wave forms from very low frequencies on up into the high frequency ranges.
(8) If suitable calibrating potentials are available it may be used as an electronic voltmeter. As an example, if it is desired to determine the voltage of an unknown signal being applied, the VERT. GAIN controls may be adjusted to give a deflection such as 15 small squares, or one and one-half inches. By substituting for the unknown voltage a known voltage of given magnitude, the ratio of the number of divisions of deflection of the unknown voltage would be proportional to that voltage as the number of divisions of deflection of the unknown voltage is to that unknown voltage. As a concrete example, if, with a given setting of the gain controls, the unknown voltage produced 15 divisions and a known voltage of 5 volts produced 5 divisions, the unknown voltage is to 15 as the known voltage (5) is to 5 divisions, or unknown voltage equals 15 volts.

If either of the VERT. GAIN controls are changed, recalibration should be effected unless notations of the exact control settings have been made and recorded for future use. Such recorded calibrations should be accurate for relatively long periods of time as they would be affected only by the operator's ability to reset accurately and the potential loss of mutual conductance with age of the vertical amplifier tubes.
(9) If using the DC vertical amplifier section with unshielded leads, caution should be taken as these unshielded leads might pick up stray fields and distort the wave shape being observed. Such precautions consist of using as short leads as possible and orienting the leads so that they do not come close to a source of AC fields such as transformers or alternating-currentcarrying wires.


Figure 4.4


Figure 4-6


Figure 4.5


Figure 4-7

Wave Forms

## SECTION 5 OPERATOR'S MAINTENANCE

## 1. PILOT LIGHT AND FUSES.

Connect power cord of Oscilloscope OS-8C/U to an outlet supplying $115 \mathrm{~V} \pm 10 \%, 50$ to 1000 cycles AC. When the oscilloscope is energized, the pilot light should glow.

If the pilot light does not light, disconnect unit from power source and check fuses. This may be done by grasping the fuse holder finger grip cap and pressing it while making a slight turn to the left then pulling out. Check continuity of the fuse element with an ohmmeter.

If the fuse is found satisfactory, replace, and check the pilot light. Grasp pilot light jewel by the knurled portion and unscrew, then press in on lamp, twist to the left and pull out. Check lamp element for continuity with an ohmmeter.

## 2. EMERGENCY MAINTENANCE.

a. OPERATORS' NOTICE.

Operators should not perform any of the emergency maintenance procedures without proper authorization. Whenever tubes are replaced, realignment is necessary and table 7-2, the Alignment Chart, must be followed.

## b. REPLACEMENT OF TUBES.

To replace tubes, remove sides, six screws per side. Tubes V101, V102, V103 and V104 are found on terminal board TB102 attached to the vertical amplifier panel (see fig. 7-3). Tubes V105, V106 and V107 are found on terminal board TB101 attached to the horizontal amplifier panel (see fig. 7-2). Tube V108 is mounted on the bracket attached to the sweep circuit oscillator panel (see fig. 7-2). Tube V110 is mounted on top of the power supply chassis (see fig. 7-3). Replacement of cathode ray tube may be accomplished by following procedure given in paragraph 1b, section 7 .

## SECTION 6

## PREVENTIVE MAINTENANCE

## 1. GENERAL.

Preventive maintenance is the removing of possible trouble which might later cause the equipment to become inoperative. Primarily, this includes periodic inspection, checking, cleaning and tightening of contacts and components. Certain suggestions can be made for such a program, but local conditions will largely determine the exact details.

The guide to the program will be found in Table 6-1 ROUTINE MAINTENANCE CHART. By carefully following this chart, troubles can be detected and remedied before causing actual breakdown of the equipment.
2. LUBRICATION.

No lubrication is required.

## 3. CLEANING.

## WARNING

Disconnect power cord.
a. GENERAL.-The chassis is best blown out with dry compressed air free of oil vapor, or cleaned with a dry cloth and a soft dry paint brush of suitable size. It
may be necessary to use dry cleaning solvent, $140 \cdot \mathrm{~F}$ FED P-S-661 Type II (SNSN G51-S-4718-10 for a 5 gallon can), on a cloth to clean ceramic high voltage insulators. On chassis surfaces, however, this solvent should not be used as there is danger of softening the tropicalizing paint which covers them. Dust should be cleaned off thoroughly, both inside and outside the case.

Inspection should be combined with cleaning, since every part of the equipment can be observed at that time, and cleaning may inadvertently break or loosen a connection.

All exposed lug and screw connections, plug and socket connections, and electron tube pins should be checked for tightness. Cable ends should be properly dressed to prevent short circuits or strain on wires and lugs.

## Caution

Faulty electrical contacts can cause equipment failure at a critical time. Evidences of heating or breakdown such as carbonized surfaces, overheated resistors with discolored surfaces, and discolored metal parts should be noted. Though there may be no damage, potential trouble is indicated.

TABLE 6-1. ROUTINE MAINTENANCE CHART

## ATTENTION OF MAINTENANCE PERSONNEL IS INVITED TO REQUIREMENTS OF CHAPTER 67 OF THE "BUREAU OF SHIPS MANUAL" OF THE LATEST ISSUE.

The following Table is given as a basis for a routine maintenance schedule.

## WARNING

Before removing the case, remove the power cable. After removal of the case, discharge any capacitors in the power supply.

MONTHLY
a. Remove fuses one at a time. Clean and burnish ends and clips as needed.
b. Check tube pins and socket contacts for corrosion. Clean as needed.
c. Check all tubes in a tube tester. Replace weak tubes.
d. Replace any tubes missing from tested emergency spares after first testing in proper socket.
e. Check operation of all panel controls.
f. Blow out dust with dry compressed air.
g. Check for rust and corrosion. Clean and touch up with paint as needed.

All knobs should be checked for looseness and tightened if necessary. Occasionally knobs become loose and fail to rotate their controls; thus, a loose knob may give the impression of fault in a variable circuit.

Rough handling of the oscilloscope will sometimes jar parts or wires out of position or abrade them; such damage should be repaired. Rust or corrosion on painted surfaces should be cleaned and sanded smooth, and the spot covered with touchup paint. Unpainted surfaces will not ordinarily corrode unless exposed to salt water or some other corrosive agent. Should corrosion occur, it should be cleaned off thoroughly, taking care not to let the scrapings fall into the unit, and the spot touched up with clear varnish or tropicalizing paint. Paint or varnish should not be used too close to switch or tube socket contacts.

## b. TUBES.

Compressed air free of oil vapor or a brush will usually suffice to remove dust from the tubes. Be careful to clean tubes that operate at a high temperature, as a layer of dust would interfere with heat radiation and raise the operating temperature. After cleaning, make sure that all tubes are properly seated in their sockets, and all tube clamps locked.

The plate connectors used on high voltage rectifier tubes may lose their spring tension as a result of overheating. The tension should be increased when necessary.

## c. FUSES.

Fuses should be removed and checked for corrosion and looseness, either of which can cause eventual trouble. A clean cloth moistened with dry cleaning solvent, 140-F FED P-S-661 Type II (SNSN G51-S-4718-10 for a 5 gallon can), will usually suffice for cleaning the fuses and clips, but in some cases it may be necessary to use crocus cloth or fine sandpaper. When repiacing, make sure that the fuses are tight in their clips.

## d. HIGH-VOLTAGE INSULATORS.

Ceramic and other insulators for voltages under 600 volts are usually tropicalized. They should be kept clean, but care should be taken not to remove the special paint. The use of solvents is not recommended.

Ceramic insulators for voltages greater than $\mathbf{6 0 0}$ volts are not tropicalized. They should be kept clean to prevent the possibility of arc-overs. It may be necessary to use a cloth moistened with dry cleaning solvent, 140-F FED P-S-661 Type II (SNSN G51-S-4718-10 for a 5 gallon can), or some other solvent.

## FAILURE REPORTS

AFAILURE REPORT must be filled out for the failure of any part of the equipment whether caused by defective or worn parts, improper operation, or external influences. It should be made on Failure Report, form NAVGEH 1025 which has been designed to simplify this requirement. The card must be filled out and forwarded to BUSHIPS. Full instructions are to be found on each card.

Use great care in filling the card out to make certain it carries adequate information. For example under "Circuit Symbol" use the proper circuit identification taken from the schematic drawings, such as T-803, in the case of a transformer, or R-207, for a resistor. Do not substitute brevity for clarity. Use the back of the card to completely describe the cause of failure and attach an extra piece of paper if necessary.

The purpose of this report is to inform BUSHIPS of the cause and rate of failures. The information is used by the Bureau in the design of future equipment and in the maintenance of adequate supplies to keep the present equipment going. The cards you send in, together with those from hundreds of other ships, furnish a store of information permitting the Bureau to keep in touch with the performance of the equipment of your ship and all other ships of the Navy.
This report is not a requisition. You must request the replacement of parts through your Officer-in-Charge in the usual manner.
Make certain you have a supply of Failure Report cards and envelopes on board. They may be obtained from the nearest District Printing and Publication Office.

# SECTION 7 <br> <br> CORRECTIVE MAINTENANCE 

 <br> <br> CORRECTIVE MAINTENANCE}

## 1. GENERAL.

Components in oscilloscope OS-8C/U can, in general, be replaced with equivalent components without the necessity of any further adjustment except where specifically mentioned. Most of the components may be replaced in the scope generally serviced by merely removing the side panels, six screws per panel; however, it will be found much more convenient when attempting any major repair to remove the subassembly involved as indicated below.
a. REMOVING SUB-ASSEMBLIES
(1) VERTICAL AMPLIFIER.
(a) Remove the right side panel.
(b) Unsolder the two leads from the vertical amplifier assembly at terminal board TB105 in the rear of the scope.
(c) Remove the four screws holding the vertical amplifier assembly to the top of the chassis.
(d) Remove the assembly from the chassis by giving it a slight counter-clockwise turn and pulling straight out.
(e) The vertical amplifier assembly may then be swung down and laid on the bench next to the oscilloscope, and the two leads from the amplifiers reconnected to the terminal board with short jumpers. The oscilloscope may now be operated in its normal manner with this circuit completely exposed.
(2) HORIZONTAL AMPLIFIER.
(a) Remove the left side panel.
(b) Unsolder the two leads from the horizontal amplifier assembly at terminal board TB105 in the rear of the scope.
(c) Remove the four screws holding the horizontal amplifier panel to the top of the chassis.
(d) Remove the assembly from the chassis by giving it a slight clockwise turn and pulling straight out.
(e) The horizontal amplifier assembly may then be swung down and laid on the bench next to the oscilloscope, and the two leads from the amplifiers reconnected to the terminal board with short jumpers. The oscilloscope may now be operated in its normal manner with this circuit completely exposed.
(3) SWEEP CIRCUIT OSCILLATOR.
(a) Remove the left side panel.
(b) Remove the four screws holding the sweep circuit oscillator panel to the top of the chassis.
(c) Remove the assembly from the chassis by pulling straight out.
(d) The sweep circuit oscillator may then be swung down and laid on the bench beside the oscillo-
scope and the scope operated in the normal manner with this circuit completely exposed.
(4) SYNC. CIRCUIT.
(a) Remove the right side panel.
(b) Remove the four screws holding the sync. circuit panel to the top of the chassis.
(c) Remove the assembly from the chassis by applying a slight clockwise twist and pulling straight out.
(d) The sync. circuit assembly may then be swung down and laid on the bench next to the scope and the scope operated in the normal manner with this circuit completely exposed.
(5) POWER SUPPLY.
(a) Disengage the bottom pan from the chassis by removing the four water-tight screws from the shock mounts.
(b) Remove both side panels.
(c) Unsolder the shield of the power cord from its lug on the power supply assembly.
(d) Unsolder wire on rear terminal of lower fuse holder and the longer wire on the a-c switch located on the back of the intensity control.
(e) Remove the four screws holding the power supply assembly to the chassis. Two of these screws are located on the front of the chassis and the other two on the bottom.
(f) The assembly may then be removed by pulling it through the opening on the right side of the chassis and turning it slightly counter-clockwise. There is sufficient slack in the cabling to permit this removal.
(g) After reconnecting the two wires by means of jumpers, the oscilloscope may be operated in the normal manner with this assembly completely exposed.

## Important Note

IN CASE OF EMERGENCY, WHEN REPLACEMENT PARTS ARE NOT AVAILABLE, THESE ASSEMBLIES MAY BE COMPLETELY DETACHED FROM THE OSCILLOSCOPE BY UNSOLDERING THE CABLES FROM DISTRIBUTION BOARD AND A CONSOLIDATION OF WORKABLE ASSEMBLIES MAY BE ACCOMPLISHED SINCE EACH ASSEMBLY IS INTERCHANGEABLE FROM ONE OSCILLOSCOPE TO ANOTHER.



Figure 7-1. Oscilloscope OS8-C/U, Sub-Assemblies Removed

NAVSHIPS 92251
OS-8C/U

## CORRECTIVE MAINTENANCE

## b. REPLACING CATHODE RAY TUBE. <br> Caution

HANDLE WITH CARE. Breakage of this tube, which contains a high vacuum, may result in injury from flying glass. Do not strike or scratch the tube. Never subject to more than moderate pressure when installing in or removing from equipment.

Should it be necessary to replace the cathode ray tube, the following procedure should be followed:
(1) Remove the right side panel.
(2) Loosen the cathode ray tube clamp (See Fig. ure 7-2).
(3) The cathode ray tube may then be removed by disengaging the socket and pulling forward and out with the tube visor.
c. REPLACING THE TRANSFORMER (See Fig. ure 7.3).

Should it become necessary to replace transformer T101, the following procedure should be followed:
(1) Disengage the bottom pan from the chassis by removing the four water-tight screws from the shock mounts.
(2) Remove both side panels.
(3) Unsolder all leads from the transformer terminals, being sure to identify them so that they can be correctly replaced.
(4) Remove the cathode ray tube as outlined above.
(5) Remove the four screws securing the transformer to the main chassis. These screws are located on the bottom of the chassis.
(6) The transformer may then be removed through the right side of the chassis and the replacement made.

## d. ALIGNMENT OF DC AMPLIFIERS (HORI-

 ZONTAL AND VERTICAL).The amplifiers used in the vertical and horizontal deflection circuits are of the direct-coupled type which depend upon proper adjustment for best operation. Although these adjustments are made in the factory, it is possible that after replacement of major components, readjustment may be required for optimum performance. Some of the symptoms of maladjustment and the methods for correcting them are listed below, as well as in Table 7-2.
(1) LACK OF SENSITIVITY, INSUFFICIENT POSITIONING, CROWDING, OR POOR FOCUS (ASTIGMATIC CONDITION)-If any one or more of these conditions exist in the vertical or horizontal amplifiers, readjustment of BIAS controls R119 and R1fl respectively would be advisable. For the vertical amplifier, adjust BIAS ADJ. R119 (See Figure 3-4) until the voltage drop across plate load resistor R123 or R124 (See Figure 7.10 is 45 volts with the beam vertically centered on the cathode ray tube. For the horizontal amplifier, BIAS ADJ. R141 (See Figure 7-3) should be adjusted until the voltage drop across plate load resistor R145 or R146 (See Figure 7-10) is 90 volts
when the beam is horizontally centered on the cathode ray tube.

If, after the bias adjustment indicated above, the vertical amplifier still exhibits excessive crowding, readjustment of LINEARITY control R121 would be advisable. Crowding is the term used for non-linearity of the pattern height with changes in positioning. For example, a one-half inch pattern obtained in the center of the screen may be appreciably less than one-half inch when positioned to the top or bottom of the screen. To readjust LINEARITY control R121, feed a test signal into the vertical amplifier and adjust the trace until it is approximately one-half inch high and positioned to the top or bottom of the cathode ray tube. Adjust R121 (See Figure 3-4) for maximum deflection.
(2) SHIFTING OF THE BEAM WITH GAIN CONTROL SETTINGS ON DC ATTENUATOR POSITION-When the vertical or horizontal attenuators are in the DC position and no signal is being fed into the DC input, the beam should not shift appreciably when the GAIN control is rotated. If the beam shifts vertically or horizontally it would be advisable to readjust potentiometers R112 (See Figure 7-2) or R135 (See Figure 7-3) respectively. The easiest way to accomplish this is to center the beam with the POSITIONING control while the GAIN control is in its extreme counter-clockwise. position, with no signal applied to the amplifier, and with the intensity reduced so as not to burn a hole in the cathode ray tube screen. Then, turn the GAIN control to its extreme clockwise position and re-center the beam with potentiometer R112 (vertical) or R135 (horizontal), depending upon whether the beam moves vertically or horizontally. This process may have to be repeated more than once.
(3) POSITIONING CONTROLS INCAPABLE OF SWINGING THE BEAM OFF SCREEN IN ONE DIRECTION-If replacement tubes used in the horizontal DC amplifier are badly unbalanced, a condition might result in which the POSITIONING control is not capable of positioning the beam off screen in one direction. If this condition arises, the unbalanced tube should be replaced. In an emergency, resistor R187 (See Figure 7-10) (horizontal) may be changed in value until the beam will swing off screen in both directions. This resistor is $560 \mathrm{~K}, 10 \%, 1 / 2$ watt, carbon, as originally supplied in the oscilloscope and any replacement should be the same type (carbon) but could range in value anywhere from 330 K to 4.7 megohm.
(4) LACK OF FREQUENCY RESPONSE, SQUARE WAVE ROUNDING, OR EXCESSIVE SQUARE WAVE OVERSHOOT (See Figures 7.4, 7.5 and 7-6)-In making any adjustments of the frequency characteristics of the amplifiers or the compensation of the attenuators, it is important that a good quality square wave generator be used in order to insure good pulse response.
-With a 100 kc square wave on the vertical amplifier, and the attenuator in the AC divide by 1 (AC-1) position, the trace should exhibit a fast rise time and about

TABLE 7-2. Alignment Chart for Major Component Replacement.

| COMPONENT REPLACED | SYMPTOMS SHOWING NEED FOR ALIGNMENT | PART <br> TO BE <br> ALIGNED | ALIGNMENT PROCEDURE |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { V102, V103 } \\ & \text { or V104 } \end{aligned}$ | Lack of Sensitivity, Insufficient Positioning, Crowding, or Poor Focus (Astigmatic Condition) on Vertical Amplifier. | Bias. Adj. R119 | Adjust R119 until drop across plate load resistor R123 or R124 is 45 volts with the beam vertically centered on the cathode ray tube. |
|  | Crowding after the bias adjustment indicated above. | Linearity Control R121 | Feed a test signal into the vertical amplifier and adjust the trace until it is approximately one-half inch high and positioned to the top or bottom of the cathode ray tube. Adjust R121 for maximum deflection. |
| $\begin{aligned} & \text { V106 or } \\ & \text { V107 } \end{aligned}$ | Lack of Sensitivity, Insufficient Positioning, Crowding, or Poor Focus (Astigmatic Condition) on Horizontal Amplifier. | Bias Adj. R141 | Adjust R141 until drop across plate load resistor R145 or R146 is 90 volts when the beam is horizontally centered on the cathode ray tube. |
| $\begin{aligned} & \text { V102 or } \\ & \text { V106 } \end{aligned}$ | Shifting of the Beam with Gain Control Settings on DC Attenuator Position. | R112 <br> (Vertical) <br> R135 <br> (Horizontal) | With the gain control counter-clockwise, center the beam wth positioning control. Then run the gain control clockwise and re-center the beam with R112 (Vertical) or R135 (Horizontal). |
| $\begin{aligned} & \text { V102, V106 } \\ & \text { or V107 } \end{aligned}$ | Positioning Controls Incapable of Swinging Beam off Screen in One Direction. |  | Replace unbalanced tube or in case of emergency change resistors R114 (Vertical) or R187 (Horizontal). |
| V102, V103, V104, V106 or V107 | Lack of Frequency response, square wave rounding, or excessive square wave overshoot in the AC divide by 1 (AC-1) attenuator position. | C109 (Vertical) or C119 (Horizontal) | With 100 KC square wave, adjust C 109 (Vertical) for $3 \%$ overshoot. With 25 KC 3 square wave, adjust C119 (Horizontal) for $\mathbf{3 \%}$ overshoot. |
| Any Attenuator Components | Square wave rounding or excessive square wave overshoot in the (AC-10) or (AC-100) attenuator positions. | C101 (Vertical AC-10) C102 (Vertical AC-100) C111 (Horizontal AC-10) C112 (Horizontal AC-100) | With square wave, adjust attenuator trimmer condensers until the trace appears normal. |



Figure 7-2. OS-8C/U,Right Side View, Cover and Side Panel Removed


Figure 7-3. OS-8 C/U,Left Side View, Cover and Side Panel Removed

3\% overshoot as indicated in Figure 7.6. If the trace exhibits rounding as in Figure 7-4, or excessive overshoot as in Figure 7.5, readjustment of trimmer condenser C109 (See Figure 7-2) would be advisable. If, after the adjustment indicated above, the square wave trace appears distorted on the AC divide by 10 (AC-10) position, adjust trimmer condenser C101 (See Figure 7-2) until the trace appears normal as in Figure 7-6. If the distortion appears on the AC divide by 100 (AC100) position, adjust C102 (See Figure 7-2) as above.

With the vertical amplifier driven by a sawtooth from an external source to provide a vertical sweep, the horizontal attenuator in the AC divide by 1 (AC-1) position, and a 25 kc square wave on the horizontal amplifier, the trace should exhibit a fast rise time and about 3\% overshoot as indicated in Figure 7.6. If the trace exhibits rounding as in Figure 7-4, or excessive overshoot as in Figure 7-5, readjustment of trimmer condenser C119 (See Figure 7.3) would be advisable. If, after the adjustment indicated above, the square wave trace appears distorted on the AC divide by 10
(AC-10) position, adjust trimmer condenser C111 (See Figure 7.3) until the trace looks normal as in Figure 7-6. If the distortion appears on the AC divide by 100 (AC-100) position, adjust trimmer C112 (See Figure 7-3) as above.
c. MAKING REPLACEMENTS WITH COMPONENT PARTS OTHER THAN THOSE CALLED FOR IN THE PARTS LIST.
(1) E101 may be made from Standard Navy Stock Number N17-P-69135-8011 by cutting off the excessive stud length.
(2) X101 and X103 may be made from Standard Navy Stock numbers N16-S-64063-6717 and N16-S-62063-6693 respectively by cutting off the ground ears and removing the center shield.
(3) When replacing X109 socket, check the color coding on replacement socket and make any necessary notes as to changes before removing the old socket.


Figure 7.4
Square wave exhibiting excessive rounding. UNDER-COMPENSATED


Figure 7-5
Square wave exhibiting excessive overshoot. OVER-COMPENSATED


Figure 7.6
Square wave exhibiting 3\% overshoof. CORRECT ADJUSTMENT




* vOLTAGE MEASUREMENTS TAKEN WITH CONTROLS IN FOLLOWING POSITIONS:-

GAIN SET AT $O$, ATTENUATOR SET AT AC $X I$.

- HOR. AMP. $\qquad$
QAIN SET AT O, ATTENUATOR SET. AT SWEEP.
——SYNC. CIRCUIT ——_
SELECTOR SET AT INTERNAL LOCKING SET AT + SO.
-SWEEP CIRCUIT OSC.-
COARSE FREQUENCY SET AT 100-475, VERNIER FREQUENCY SET AT O.
FRONT PANEL CONTROLS SET FOR LOW INTENSITY FOCUSED SPOT IN CENTER OF SCREEN.
D.C.V. READINGS WERE TAKEN WITH A 20,000 $\Omega$ PER VOLT METER. A.C.V. READINQS WERE TAKEN WITH A I,000 $\Omega$ PER VOLT METER. ALL TEST LEADS DISCONNECTED.
RESISTANCE MEASUREMENTS TAKEN WITH CONTROLS IN POSITION FOR VOLTAGE MEASUREMENTS BUT WITH LINE POWER CORD REMOVED.


ALL OTWER VOLTAEES ANO MESISTance neapimes mace TO EnOUNO.


## T-IOI

POWER TRANSFORMER


* BETWEEN PINS $1+2$ 115 VAC. $7 \Omega$
+BETWEEN PINS $8+96.3$ VAC, $0.4 \Omega$
READING ON ALL OTHER TEMINALS TO GND.
ACV READ WITH IOOO $\Omega$ PER VOLT METER, LINE VOLTAGE IIS V.,CONTROLS SET AS IN FIG. 7-7.

Figure 7-8. Power Transformer Voltage and Resistance Measurements


TBIO3
DISTRIBUTION BOARDS
TBIO4


| $N O$. | $\Omega$ | $V$ |
| :---: | :---: | :---: |
| 1 | $0-500$ | 1.2 |
| 2 | 0 | 3.15 AC |
| 3 | 0 | 3.15 AC |
| 4 | 50 K | 107 |
| 5 | 1.5 M | -560 |
| 6 | 3 M | -500 |
| 7 | - | -560 |
| 8 | 80 K | +280 |
| 9 | - | -560 |
| 10 | 150 K | +130 |
| 11 | 12 K | +97 |
| 12 | 1 M | +0.4 |
| 13 | 20 K | +7.5 |
| 14 | 125 K | +90 |
| 16 |  |  |
| 16 | 470 | .8 |
| 17 | 0 | 0 |
| 18 | 175 K | 235 |


| $N O$. | $\Omega$ | $V$. |
| :---: | :---: | :---: |
| 19 | 80 K | +80 |
| 20 | 1.5 M | -560 |
| 21 | 50 K | +107 |
| 22 | 0 | 3.15 AC |
| 23 | 0 | 3.15 AC |
| 24 | $0-500$ | +1.2 |
| 25 | $0-500$ | +1.0 |
| 26 | 220 K | 0 |
| 27 | 90 K | +320 |
| 28 | 100 K | +120 |
| 29 | 1.4 M | -510 |
| 30 | 1.5 M | -510 |
| 31 | 1 M | -340 |
| 32 | 470 | +.7 |
| 33 | 470 | +.7 |
| 34 | 100 K | +340 |
| 35 | 0 | 0 |
| 36 | 20 K | +8 |

+ BETWEEN PINS $7+96.3$ VAC., $8 \Omega$.
ALL OTHER VOLTAGES AND RESISTANCES TO GND.
ACV READ WITH $1000 \Omega$ PER VOLT METER, DCV READ WITH 20,000 ת PER VOLT METER, LINE VOLTAGE IIS V.,CONTROLS SET AS IN FIG. 7-7.

Figure 7. 9. Distribution Board Voltage and Resisfance Measuremants



## SECTION 8 <br> PARTS LISTS

## 1. SUPPLEMENTARY TABLE.

Part numbers in the parts list section have been corrected and deletions have been made by means of Supplementary Tables 8-1A and 8-1B below. Always refer to Supplementary Tables 8-1A and 8-1B for the part number for a given item as it completely supersedes any corresponding part number in the basic Table of Replaceable Parts. If no part number is shown for a given item, refer to the basic table for the part number.

## 2. STOCK NUMBERS.

The stock numbers and support information that appear in this section have been revised. For Federal Stock Numbers and Source Maintenance and Recoverability Codes refer to the appropriate Stock Number Identification Table issued by the Electronics Supply Office. The SNIT, rather than this publication, shall govern if there is any conflict in stock numbers and support information.

TABLE 8-1. LIST OF MAJOR UNITS

| sYmBOL GROUP | QUANTITY | NAME OF MAJOR UNIT | DESIGNATION |
| :---: | :---: | :---: | :---: |
| 100 | 1 | Oscilloscope | OS-8C/U |

SUPPLEMENTARY TABLE 8-1A. CHANGE DATA FOR TABLE OF REPLACEABLE PARTS*

| $\begin{gathered} \text { REF. } \\ \text { DESIG. } \end{gathered}$ | NEW PART NUMBER' | $\begin{gathered} \text { REF. } \\ \text { DESIG. } \end{gathered}$ | NEW PART NUMBER' | $\begin{gathered} \text { REF. } \\ \text { DESIG. } \end{gathered}$ | NEW PART NUMBER $\dagger$ | REF. DESIG. | NEW PART NUMBER $\dagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A-101 | C644-13 | O-101 | A644-45 | S-103 | A644-24 | TB-105 | A644-33 |
| A-102 | E644-87 | O-102 | B644-74 | S-104 | A644-21 | TB-106 | A644-106 |
| A-121 | Delete | O-103 | C644-86 | T-101 | C644-84 | W-101 | A644-54 |
| A-124 | Delete | O-104 | A644-46 | TB-101 | A644-48 | W-102 | A644-54 |
| E-110 | Delete | O-105 | Delete | TB-102 | A644-47 | W-103 | A644-43 |
| E-113 thru E-122 | Delete | S-101 | A644-22 | TB-103 | A644.49 | W-104 | A644-91 |
| H-101 | A644-44 | S-102 | A644-23 | TB-104 | A644-50 |  |  |
| ${ }^{*}$ The data in this table apply only to Oscilloscopes OS-8C/U with serial numbers 8,633 hrough 10,210 and 14,163 through 14,249 , manufactured by Polytronic Researeh, Inc. 326 Westmore Road, Rockville, Md. <br> †In the "New Part Number" column, all part numbers are those of Polytronic escarch, Inc. The word "Delete" indicates that the part is not used in the equipment vered by this Change. |  |  |  |  |  |  |  |

## SUPPLEMENTARY TABLE 8-1B. CHANGE DATA FOR table Of replaceable parts*

| $\begin{gathered} \text { REF. } \\ \text { DESIG. } \end{gathered}$ | NAME OF PART AND DESCRIPTION |
| :---: | :---: |
| A-101 | Size 13-3/4-in. lg., 6-15/16-in. wide, 9 -in. high overall . . . Carol 32-2150. |
| A-102 | CHASSIS, . . . secured by 6-32 x 3/8 pan-hd screws. Carol 32-3054. |
| A-103 | Carol 32-640-1. |
| A105 | Carol 32-640-2. |
| A121 | Carol 32-546. |
| A-124 | Carol 32-545. |
| C-101 | 6-30 uuf capacity; Centralab part no. 821-AN-2. |
| C-102 | CAPACITOR, VARIABLE, CERAMIC DIELECTRIC; rotary type, 3-12 uuf capacity, Centralab part no. DA-821-013. |
| C-103 | 100 uuf $\pm 2 \%$; MIL Spec C-20, type CC32CG101E. |
| C-104 | CAPACITOR, FIXED, MICA DIELETRIC; 1000 uf $\pm 10 \%$; 300 V DCW, CM20B102K per MIL-C-5. |
| C-105 | CAPACITOR, FIXED, PLASTIC DIELECTRIC, 1 section, 250,000 uff, $+20 \%$; 400 V DCW; plastic case; 0.675 dia. x 1-1/2-in. lg., Pyramid type 107. |
| C-106 | Sprague part no. M17998. |
| C-107 | 4700 uff CK62Y472Z per MIL-C-11015A. |
| C-111 | Same as C102. |
| C-112 | Same as C102. |
| C-116 | 50 uf; 6V DCW; Cornell-Dubilier part no. BBR-50-6. |
| C-119 | Same as C102. |
| C-120 | CP05A1EC154K per MIL-C-25A. |
| C-122 | CAPACITOR, FIXED, PLASTIC DIELECTRIC: 1 section, 0.453 dia. x $7 / 8-\mathrm{in}$. $\lg$., 150,000 uuf $\pm 20 \%$; 200 VDCW; Pyramid type 167. |
| C-124 | CAPACITOR, FIXED, PLASTIC DIELECTRIC, 1 section; 500,000 uf $\pm 10 \% ; 200 \mathrm{~V}$ DCW; 0.609. dia. x 1-3/8-in. lg., Pyramid type 107 .' |
| C-126 | Same as C122. |
| C-127 | CAPACITOR, FIXED, PLASTIC DIELECTRIC; 1 section; 30,000 uf $\pm 20 \%$; 200V DCW, low-loss plastic case; $1 / 4$-in. dia. x $3 / 4$-in. lg.; Pyramid type 107. |
| C-128 | CAPACITOR, FIXED, MICA DIELECTRIC; 5100 uuf $\pm 10 \%$; 300V DCW ; CM35D513J per MIL-C-5. |
| C-130 | 150 uuf $\pm 2 \%$; CC35CG151G per MIL-C-20B. |
| C-131 | 51 uuf $\pm 2 \%, \mathrm{CC} 25 \mathrm{CH} 510 \mathrm{G}$ per MIL-C-20B. |
| C-132 | Electra Mfg. Co., No. 12E202MA5. |
| C-136 | 100,000 uuf $\pm 20 \%$. |
| C-137 | CAPACITOR, FIXED, PLASTIC DIELECTRIC, 100,000 uuf $\pm 20 \%$; 400V DCW; 0.421-dia. x 1-in. lg.; Pyramid type 107. |
| C-141 | Same as C-137. |
| C-142 | CAPACITOR, FIXED, MICA DIELECTRIC; 25 uuf $\pm 10 \%$; 500V DCW; CM15B250K per MIL-C-54. |
| CR-101 | $3 / 4-\mathrm{in} . \mathrm{lg}$. x 3/4-in. wide; International Rectifier No. 59-0718. |
| CR-103 | International Rectifier No. 61-4325. |
| E-111 | FHN20G per MIL-F-19207. |
| E-113 th | E-122-Deleted |
| E-123 | TS102U02 per JAN-S-28A. |
| E-124 | TS102U03 per JAN-S-28A. |
| F-101 | 2 amp ; MIL F20D2ROOB. |
| H-101 | Carol no. 32-554. |
| I-101 | LAMP, INCANDESCENT; 6-8 volts, 0.15 amps , MS-15571-2. |
| 0-101 | Carol no. 32-555. |
| 0-102 | Carol no. 32-1246. |
| -103 | Carol no. 32-2134. |
| O-104 | Butyrate acetate scale; Carol no. 32-557. |
| O-105 | Carol no. 32-577. |
| 0-106 | $3 / 8-\mathrm{in}$. height of head. |

[^0]
## SUPPLEMENTARY TABLE 8-1B. CHANGE DATA FOR TABLE OF REPLACEABLE PARTS*

| $\begin{gathered} \text { REF. } \\ \text { DESIG. } \end{gathered}$ | NAME OF PART AND DESCRIPTION |
| :---: | :---: |
| 0-113 | Kurz-Kasch part no. S-202-32, w/2 set screws. |
| 0-117 | Same as 0-113. |
| 0-118 | Same as 0-113. |
| 0-119 | Same as 0-113. |
| 0-120 | Same as 0-113. |
| O-125 | Carol no. 32-622. |
| R-104 | Carol no. 32-703. |
| R-109 | 100 megohms $\pm 10 \%$; RC20GF107K per MIL-R-11B. |
| R-110 | 390 ohms $\pm 5 \%$; RC20GF391J per MIL-R-11B. |
| R-111 | Carol no. 32-710. |
| R-114 | Deleted. |
| R-116 | 3,600 ohms $\pm 5 \%$; RC20GF362J per MIL-R-11B. |
| R-119 | Carol no. 32-714. |
| R-120 | 4700 ohms $\pm 10 \%$; RC20GF472K per MIL-R-11B. |
| R-121 | Carol no. 32-713. |
| R-133 | RESISTOR, FIXED, COMPOSITION; 10 megohms $\pm 10 \% ; 1 / 2 \mathrm{~W}$; RC20GF106K per MIL-R-11B. |
| R-154 | Carol no. 32-710. |
| R-166 | Same as R-151. |
| R-176 | Carol no. 32-712. |
| R-177 | Carol no. 32-710-3. |
| R-181 | RESISTOR, FIXED, COMPOSITION; 120,000 ohms, $\pm 10 \% ; 1 / 2 \mathrm{~W}$; RC20GF124K per MIL-R-11B. |
| R-187 | 560,000 ohms $\pm 10 \%$; RC20GF564K per MIL-R-11B. |
| R-189 | Same as R-149. |
| R-190 | Same as R-120. |
| S-101 | Carol no. 32-501. |
| S-102 | Carol no. 32-502. |
| S-103 | Carol no. 32-503. |
| S-104 | Carol no. 32-500. |
|  | TRANSFORMER, POWER, STEP DOWN AND STEP UP: Hermetically sealed, fully enclosed metal case; primary winding (term. 1 to 2) $115 \mathrm{v}, 50$ to 1000 cycles, single phase; secondary winding no. 1 (term. 3 to 4) $220 \mathrm{v}, 60$ ma; no. 2 (term. 4, 12,5) $220 \mathrm{v}, 76$ ma centertapped; no. 3 (term. 5 to 6) 220 v , 60 ma ; no. 4 (term. 6 to 7) $140 \mathrm{v}, 0.5 \mathrm{ma}$; no. 5 (term. 10 to 11) $6.3 \mathrm{v}, 3.75$ amp. centertapped; No. 6 (term. 8 to 9) $6.3 \mathrm{v}, 0.6 \mathrm{amp}$; 2000 volt insulation, asphalt-filled; dimensions excluding terminals and mfg. brackets 3 in. lg. $\times 2-15 / 32$ in. wide $\times 2-27 / 32 \mathrm{in}$. high; 2-3/8 in. shortest mfg. dim.; 3-1/4 in. longest mfg. dim.; 12 insulated solder lug terminals; four no. 6.32 mfg. bushings on $3-1 / 4 \mathrm{in}$. by $2-3 / 8 \mathrm{in}$. mtg. centers; TFIRYO3YY dwg. no. 32-2115B Carol Electronics Part no. CA1104-1. |
| TB-101 | Carol no. 32-579. |
| TB-102 | Carol no. 32-578. |
| TB-103 | Carol no. 32-580. |
| TB-104 | Carol no. 32-581. |
| TB-105 | Carol no. 32-531. |
| TB-106 | Carol no. 32-701. |
| V-101 | Type 12AT7WA. |
| V-103 | Type 6AH6. |
| V-107 | Type 6J6WA. |
| V-109 | Type 3RP1. |
| V-110 | Type 6X4W. |
| W-101 | Carol no. 32-622-601. |
| W-102 | Carol no. 32-622-602. |
| W-103 | Carol no. 32-553. |
| W-104 | Carol no. 32-632. |
| X-101 | TS103PO2 per JAN-S-28A. |
| X-103 | TS103PO3 per JAN-S-28A. |
| X-108 | TS103PO1 per JAN-S-28A. |
| X-109 | Carol no. 32-474. |





| REF. <br> DESIG. | NAME OF PART AND DESCRIPTION | STOCK NOS. | SIG. CORPS STD. NAVY AIR CORPS | LOCATING FUNCTIONS |
| :---: | :---: | :---: | :---: | :---: |
| C-106 | CAPACITOR, FIXED, ELECTROLYTIC; 25 $\mathrm{mfd}-10 \%+75 \%$; 25 V DCW; insulated, vinyl sleeve; $3 / 8 \mathrm{in}$. dia. $x$ 1-1/8 in. lg.; 2 wire leads; Sprague part no. D17997. | $\begin{aligned} & \text { 3DB25-136 } \\ & \text { N16-C-19781-4701 } \\ & 055725092 \end{aligned}$ |  | Blocking cap. cathode V-101A. |
| C-107 | CAPACITOR, FIXED, CERAMIC DIELECTRIC; 5000 mmf GMV; 500V DCW; insulated, phenolic jacket; $3 / 8 \mathrm{in}$. dia. x 5/32 in. thick; 2 wire leads; Centralab part no. DA-048-001B. | $\begin{aligned} & \text { 3DA5-229 } \\ & \text { N16-C-19011-7701 } \end{aligned}$ |  | By-pass cap. plate V-101A. |
| C-108 | CAPACITOR, FIXED, ELECTROLYTIC; 1 section; $250 \mathrm{mfds} ; 6 \mathrm{~V}$ DCW tubular metal case, hermetically sealed; $5 / 8 \mathrm{in}$. dia. x $1-7 / 16 \mathrm{in}$. lg.; 2 wire leads located on ends; CornellDubilier type BRV-6025-1. | $\begin{aligned} & \text { 3DB250-8 } \\ & \text { N16-C-20503-1450 } \end{aligned}$ |  | Cathode by-pass capacitor for first vert. DC amp V-102. |
| C-109 | CAPACITOR, VARIABLE, CERAMIC DIELECTRIC; rotary type, 1 section, zero temp. coef; 2.5 mmf min, 7 mmf max capacity; 600 V DCW; 17/32 in. dia. x 9/32 in. thick; 2 solder lug terminals located on bottom; mtd. through solder lugs; screwdriver slot adjustment; ceramic base; Centralab type no. DA-821-019. | $\begin{aligned} & \text { 3D9007V-25 } \\ & \text { N16-C-63918-8658 } \end{aligned}$ |  | Adjustable freq. compensating cap. for first vert. DC amp V-102. |
| C-110 | CAPACITOR, FIXED, PAPER DIELECTRIC; Same as C-105. |  |  | Blocking cap. for horizontal AC input. |
| C-111 | CAPACITOR, VARIABLE, CERAMIC DIELECTRIC; Same as C-101. |  |  | Adjustable freq. compensating cap. for AC10 position HOR. ATTEN. |
| C-112 | CAPACITOR, VARIABLE, CERAMIC DIELECTRIC; Same as C-101. |  |  | Adjustable freq. compensating cap, for AC100 position HOR. ATTEN. |
| C-113 | CAPACITOR, FIXED, CERAMIC DIELECTRIC; Same as C-104. |  |  | Fixed freq. compensating cap. for sweep cidcuit osc. V-108 decoupling network. |
| C-114 | CAPACITOR. FIXED, CERAMIC DIELECTRIC; Same as C-103. |  |  | Fixed freq. compensating cap. for AC-10 position HOR. ATTEN. |
| C-115 | CAPACITOR, FIXED, CERAMIC DIELECTRIC; Same as C-104. |  |  | Fixed freq. compensating cap, for AC-100 position HOR. ATTEN. |
| C-116 | CAPACITOR, FIXED, ELECTROLYTIC; 1 section; 250 mfds; 25 V DCW; tubular metal case, hermetically sealed; dimensions $7 / 8 \mathrm{in}$. dia. $x$ 1-11/16 in. lg.; 2 wire leads located on ends; metal mtg. strap, one $5 / 32 \mathrm{in}$. dia. hole in mtg. strap end; Cornell-Dubilier part no. BRV-2525-2. | $\begin{aligned} & \text { 3DB250 } \\ & \text { N16-C-20506-5841 } \end{aligned}$ |  | Blocking cap. cathode V-105A horizontal cathode follower. |


|  |  |  |  |  | 号 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
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NAVSHIPS 92251
PARTS LISTS



|  |  |
| :---: | :---: |


| C-134A | CAPACITOR. <br> Part of C-134. | FIXED | ELECT |
| :---: | :---: | :---: | :---: |
| C-134B | CAPACITOR. <br> Part of C-134. | FIXED | ELEC |
| C-134C | CAPACITOR. <br> Part of C-134. | FIXE | ELEC |
| C-134D | CAPACITOR, Part of C-134. | FIXED | ELEC |
| C-135 | CAPACITOR. sections; 20 mf lar metal case; in. lg.; 3 solder cated on bottom radius; twist lu ture and fungu no. AHF 450/2 | IXED, per sect imension 90 degre mountin proofing 20-20. | ECTRO <br> -3/8 in. <br> ls, $5 / 8$ sprayed quer; A |
| C-135A | CAPACITOR. <br> Part of C-135. | FIXE | ELEC? |
| C-135B | CAPACITOR, <br> Part of C-135. | FIXE | ELEO |
| C-135C | CAPACITOR. <br> Part of C-135. | FIXEI | ELEC |
| C-136 | CAPACITOR, TRIC; 100,000 lated; phenolic 27/32 in. wide; part no. DA-93 | $\begin{aligned} & \text { IXED } \\ & \text { mimf GM } \\ & \text { lip; } 1-9 / 3 \\ & \text { wire leas } \\ & -001 \mathrm{H} . \end{aligned}$ | RAMIC ;600V D <br> in. lg., $1 /$ <br> erminals. |
| C-137 | CAPACITOR, TRIC; 100,000 case, durrz sea lg.; 2 wire lead impregnated; P92ZN. | FIXED, $\mathrm{mmf} \pm 20$ d ends; erminals astic fill | PAPER 400V D <br> in. dia. <br> cated on <br> ; Aerovo |
| C-138 | CAPACITOR, TRIC; Same a | $\begin{aligned} & \text { FIXED, } \\ & \text { C-137. } \end{aligned}$ | PAPER |
| C-139 | CAPACITOR, TRIC; Same | $\begin{aligned} & \text { FIXED, } \\ & \text { C-137. } \end{aligned}$ | PAPER |
| C-140 | CAPACITOR, TRIC: Same | $\begin{aligned} & \text { FIXED, } \\ & \text { C-137. } \end{aligned}$ | PAPER |


| REF. DESIG. | NAME OF PART AND DESCRIPTION | STOCK NOS. | SIG. CORPS <br> STD. NAVY <br> AR CORPS | LOCATING FUNCTIONS |
| :---: | :---: | :---: | :---: | :---: |
| CR-101 | RECTIFIER, METALLIC; selenium; single phase, halfwave circuit; single phase 130 V AC RMS max. input; halfwave 125 V DC 20 ma max. output; $1 / 2 \mathrm{in} . \lg$., $1 / 2 \mathrm{in}$. wide, $9 / 16 \mathrm{in}$. high over-all; center mtg. hole for 6-32 screw; 2 solder lug terminals; Radio Receptor type type "Selectron 8Y1". | $\begin{aligned} & \text { 3H4860-229 } \\ & \text { N17-R-51401-8431 } \\ & 688000-1265 \end{aligned}$ |  | Low voltage rectifier. |
| CR-102 | RECTIFIER, METALLIC; Same as CR-101. |  |  | Low voltage rectifier. |
| CR-103 | RECTIFIER, METALLIC; selenium; single phase, half-wave; single phase 1650 V AC input; 800V DC 1.5 ma max. output; 2-1/4 in. lg., .250 dia. over-all; 2 wire lead terminals; Conant part no SEIH45-TUA. | $\begin{aligned} & \text { 3H4860-230 } \\ & \text { N17-R-51557-1075 } \\ & 688000-1215 \end{aligned}$ |  | High voltage rectifier. |
| E-101 | POST, BINDING; phenolic, natural finish; $7 / 8 \mathrm{in}$. over-all height of post above mtg. surface (fully extended), $1 / 2 \mathrm{in}$. OD of post; 5/16 in. lg., $6-32$ mtg. stud; $3 / 32 \mathrm{in}$. max. dia. of wire hole; Eby type "Ensign" no. 7695 w/5/16 in. stud. | $\begin{aligned} & \text { 3Z737-25.3 } \\ & \text { N17-P-69142-3661 } \end{aligned}$ |  | Vertical amp GND connection. |
| E-102 | POST, BINDING; Same as E-101. |  |  | Vertical amp DC input connection. |
| E-103 | POST, BINDING; Same as E-101. |  |  | Horizontal amp AC input connection. |
| E-104 | POST, BINDING; Same as E-101. |  |  | Horizontal amp GND connection. |
| E-105 | POST, BINDING; Same as E-101. |  |  | Horizontal amp DC input connection. |
| E-106 | POST, BINDING; Same as E-101. |  |  | Line test output connection. |
| E-107 | POST, BINDING; Same as E-101. |  |  | Z AXIS input connection. |
| E-108 | POST, BINDING; Same as E-101. |  |  | EXT sync. connection. |
| E-109 | LAMP, INCANDESCENT; 6 to 8 volts, .15 amp; miniature bayonet base; T-3-1/4 clear bulb, white, 1 tungsten C-2 filament; $1-1 / 8 \mathrm{in}$. max. over-all height; 25 hr . rated life; any burning position; GE type 47F. | $\begin{aligned} & \text { 2Z5952 } \\ & \text { G17-L-6297 } \end{aligned}$ |  | Pilot lamp. |
| E-110 | TERMINAL, STUD; 3500V AC RMS; solder connection; brass, cadmium plated; 29/64 in. lg., $5 / 32$ in. hex. base, over-all; mts by threaded shank 2-56 thd, 7/32 in. lg.; Garde Type M3550-1. | 3Z12101-43.2 <br> Low failure item ESO ref. NavShip | required req. from 180A | Insulated terminal for components junction |

$\stackrel{\text { 3Z3282-11.19 }}{\mathrm{N} 17-\mathrm{F}-74266-9053}$

## 先

2Z8304-270
N16-S-34557-8351
774000-1955
2Z8340.277
N16-S.34607-6039
774000-1975
Overload protection.
Holds fuse F-101.
Insulated terminal for components junction.


Overload protection
Retainer for

| ${ }^{\text {E-111 }}$ | FUSE HOLDER; extractor post type; 250V, 15 amp ; accommodates 1 cartridge type fuse, $1-1 / 4 \mathrm{in} .1 \mathrm{~g} ., 1 / 4 \mathrm{in}$. dia.; molded black phenolic body; clip type beryllium copper contact, nat in . dia.; 2 solder lug terminals; mounts in single $1 / 2 \mathrm{in}$. dia. hole; Littlefuse Type A342003. | $\begin{aligned} & \text { 3Z3282-11.19 } \\ & \text { N17-F-74266-9053 } \\ & \hline \end{aligned}$ | Holds fuse F-101. |
| :---: | :---: | :---: | :---: |
| E-112 | FUSE HOLDER; Same as E-111. |  | Holds fuse F-102. |
| E-113 | TERMINAL STUD; 5000V max electrical rating; solder connection; brass, cadmium plat finish; $13 / 16 \mathrm{in} .1 \mathrm{~g} ., 5 / 16 \mathrm{in}$. hex. base, over-all dim.; mts by threaded shank $6-32,1 / 4 \mathrm{in}$. lg .; Precision Metal Type 5000. | $\begin{aligned} & \text { 3Z12101-65 } \\ & \text { N17-T-28214-4116 } \\ & \hline \end{aligned}$ | Insulated terminal for mtg. CR-103. |
| E-114 | TERMINAL, STUD; Same as E-113. |  | Insulated terminal for mtg. CR-103. |
| $\left\|\begin{array}{l} \mathrm{E}-115 \\ \text { through } \\ \text { E-122 } \end{array}\right\|$ | TERMINAL, STUD; Same as E-110. |  | Insulated terminal for components junction. |
| E-123 | SHIELD, ELECTRON TUBE; accommodates RMA envelope type T-5-1/2, straight cylinder shape with flared end, open top; brass; $1-3 / 4$ in. Ig., $3 / 4$ in. dia.; mts. on shock shield base; 2 spring shields; Eby part no. 9701-20. | $\begin{aligned} & \text { 2Z8304-270 } \\ & \text { N16-S-34557-8351 } \\ & 774000-1955 \end{aligned}$ | Shield for V-108. |
| E-124 | SHIELD, ELECTRON TUBE; accommodates RMA envelope type T-5-1/2, straight cylinder shape with flared end, open top; brass; 2-1/4 in . Ig., $3 / 4 \mathrm{in}$. dia.; mts. on shock shield base; 2 spring shields; Eby part no. 9702-11. | $\begin{aligned} & \text { 2Z8340.277 } \\ & \text { N16-S.37607-6039 } \\ & \text { 774000-1975 } \end{aligned}$ | Shield for V-110. |
| F-101 | FUSE, CARTRIDGE; $3 / 4 \mathrm{amp}, 250$ volts: time decay, blowing time 1 hr . at $135 \%$ rated load, 60 seconds max. for $200 \%$ load; ferrule type terminals, $1 / 4 \mathrm{in}$. dia. $\times 1 / 4 \mathrm{in} .1 \mathrm{~g} . ;$ glass body, enclosed type; one time; over-al dim. $1-1 / 4 \mathrm{in} . \lg . x 1 / 4 \mathrm{in}$. dia.; Littlefuse part no. 313.750 . | $\begin{aligned} & \text { 3Z2600A } 7.3 \\ & \text { N17-F-14310-370 } \end{aligned}$ | Overload protection. |
| F-102 | FUSE, CARTRIDGE; Same as F-101. |  | Overload protection. |
| F-103 | FUSE, CARTRIDGE; Same as F-101. |  | Spare fuse. |
| F-104 | FUSE, CARTRIDGE; Same as F-101. |  | Spare fuse. |
| H-101 | RETAINER, ELECTRON TUBE; no. 15 gauge stainless steel music wire; over-all dim. $1-27 / 32 \mathrm{in}$. lg., approx. $2-1 / 8 \mathrm{in}$. wide, approx. $\mathrm{x} 13 / 16 \mathrm{in}$. dia. over-all; mtd. by .136 in . dia. hole formed by end of retainer; Jetronic part no. A-554. | $\begin{gathered} \text { N16-R-503580-280 } \\ \hline \end{gathered}$ | Retainer for V-101. |


|  | TABLE 8-2. | TABLE OF REPLAC | PARTS (Cont |  | 容 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{c\|} \hline \text { REF. } \\ \text { DBSIG. } \end{array}$ | NAME OF PART AND DESCRIPTION | STOCK NOS. | SIG. CORPS <br> STD. NAYY <br> AlR CORPS | LOCATING FUNCTIONS | - |
| H-102 | RETAINER, ELECTRON TUBE; Same as H-101. |  |  | Retainer for V-102. |  |
| H-103 | RETAINER, ELECTRON TUBE; Same as H-101. |  |  | Retainer for V-103. |  |
| H-104 | RETAINER, ELECTRON TUBE; Same as H-101. |  |  | Retainer for V-104. |  |
| H-105 | RETAINER, ELECTRON TUBE; Same as H-101. |  |  | Retainer for V-105. |  |
| H-106 | RETAINER, ELECTRON TUBE; Same as H-101. |  |  | Retainer for V-106. |  |
| H-107 | RETAINER, ELECTRON TUBE; Same as H-101. |  |  | Retainer for V-107. |  |
| I-101 | LIGHT, INDICATOR; supplied w/lens $1 / 2 \mathrm{in}$. dia., red, smooth face, frosted back; friction mtd. lens holder; 1 T-3-1/4 lamp, miniature bayonet base; brass frame, nickel plated; overall dim. 2-5/32 in. lg., $15 / 16 \mathrm{in}$. dia.; mtd. through $11 / 16 \mathrm{in}$. dia. panel hole, $1 / 4 \mathrm{in}$. max. panel thickness; lamp replaceable from front; 2 solder lug terminals located on lampholder, both insulated from frame; Drake type no. 80MIL Ruby. | $\begin{aligned} & \text { 2ZK5991-7 } \\ & \text { N17-L-76854-4041 } \end{aligned}$ |  | Indicates power on. | 8 |
| I-101A | SOCKET; Part of I-101. |  |  |  |  |
| I-101B | LENS; Part of I-101. |  |  |  |  |
| J-101 | CONNECTOR, RECEPTACLE; 1 rd female contact; not polarized or grounded; straight type; 712 in . Ig., $11 / 16 \mathrm{in}$. wide, 11/16 in. high over-all, excluding protruding contacts and terminals; cylindrical body, brass, silver piated, locking type; molded polystyrene insert; Waltham part no. UG-290A/U. | $\begin{aligned} & \text { 2Z7390-290 } \\ & \text { N17-C-73108-1253 } \end{aligned}$ |  | Vert. amp AC input connection. |  |
| 0-101 | CLAMP, ELECTRICAL; steel, cadmium plated; 1 bolt type fastening device; $2-1 / 2 \mathrm{in}$. lg., $5 / 8 \mathrm{in}$. wide, 2 in . high over-all; mounted by 2.1495 in . dia. holes in ends of band; designed to hold material 1-7/8 in. max. dia. and 1-9/16 in. min. dia.; Jetronic part no. A-555. | $\begin{aligned} & \text { 2Z2642.882 } \\ & \mathrm{N} 17-\mathrm{C}-789978-709 \\ & \hline \end{aligned}$ |  | Tension clamp for cathode ray tube V-109 |  |



| TABLE 8 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { REF. } \\ & \text { DESIG. } \end{aligned}$ | NAME OF PART AND DESCRIPTION | STOCK NOS. | SIG. CORPS STD. NAVY AR CORPS | LOCATING FUNCTIONS |  |
| 0-113 | KNOB; black phenolic, w/single pointer; plain gripping surface; $1-1 / 4 \mathrm{in} . \lg ., 3 / 4 \mathrm{in}$. wide, $5 / 8$ in. thk over-all: white depressed radial line marking; Kurz-Kasch part no. S-292-3L, W/1 set screw. | $\begin{aligned} & \text { 2Z5822-13.1 } \\ & \text { N16-K-700065-545 } \\ & 292221362 \end{aligned}$ |  | VERT. ATTEN. switch knob. |  |
| 0-114 | KNOB; Same as 0-113. |  |  | COARSE FREQUENCY switch knob. |  |
| 0-115 | KNOB; Same as 0-113. |  |  | SYNC. SELECTOR switch knob. |  |
| 0-116 | KNOB; Same as 0-113. |  |  | HOR. ATTEN. switch knob. |  |
| 0-117 | KNOB; black phenolic w/single pointer; plain gripping surface; $1-1 / 4 \mathrm{in}$. Ig., $3 / 4 \mathrm{in}$. wide, $5 / 8 \mathrm{in}$. thk. over-all; 2 set screw holes 8-32; white depressed radial line marking; KurzKasch part no. S-292-3L, W/2 set screws. | 2Z5822-13.1 <br> For replacement us 545 $\qquad$ | SN N16-K-700065- | VERT. GAIN control knob. |  |
| 0-118 | KNOB; Same as 0-117. |  |  | HOR. GAIN control knob. |  |
| 0-119 | KNOB; Same as 0-117. |  |  | VERNIER FREQUENCY control knob. |  |
| 0-120 | KNOB; Same as 0-117. |  |  | LOCKING control knob. |  |
| 0-121 | KNOB; black phenolic; positive gripping surface; $9 / 16 \mathrm{in}$. Ig. over-all; 41/64 in. max. outside dia.; accommodates unthreaded shaft, $1 / 4$ in. dia.; w/brass insert; two $8-32$ set screws; Kurz-Kasch part no. S-230-64, W/2 set screws. | $\begin{aligned} & \text { 2Z5842-12 } \\ & \text { N16-K-700277-371 } \\ & \text { 292241494 } \end{aligned}$ |  | VERT. POS. control knob. |  |
| 0-122 | KNOB; Same as 0-121. |  |  | FOCUS control knob. |  |
| 0-123 | KNOB; Same as 0-121. |  |  | INT. control knob. |  |
| 0-124 | KNOB; Same as 0-121. |  |  | HOR. POS. control knob. |  |
| 0-125 | CLIP, ELECTRICAL; alligator type; steel; cad. plated; $2-11 / 32 \mathrm{in}$. lg., $3 / 8 \mathrm{in}$. wide, $5 / 16$ in. high over-all; red phenolic insulation; 5/16 in. max. jaw opening; Mueller part no. 60-HSRed (MOD) per Jetronic dwg. A-622. | $\begin{aligned} & \text { 3Z1087-8 } \\ & \text { N17-C-802585-161 } \end{aligned}$ |  | Part of test lead W-101. |  |
| 0-126 | CLIP, ELECTRICAL; Same as $\mathbf{0 - 1 2 5}$. |  |  | Part of test lead W-102. |  |

Part of test lead W-104.
Part of test lead W-104.
Part of test lead W-101.
Part of test lead W-102.
Part of voltage divider network for input of
vertical cathode follower V-101A.
Part of voltage divider network for input of
vertical cathode follower V-101A.
Vertical gain control for AC signals.
Part of voltage divider network for input of
vertical cathode foilower V-101A.
Vertical gain control.

| 10-127 | CLIP, ELECTRICAL; alligator type; steel; cad. plated; 2-11/32 in. 1g., $3 / 8 \mathrm{in}$. wide, $5 / 16$ in. wide, $5 / 16 \mathrm{in}$. high; black phenolic insulation; $5 / 16$ in .max. jaw opening; Mueller part no. 60-HS-Black. | $\begin{aligned} & \text { 3Z1087-8.1 } \\ & \text { N17-C-802584-284 } \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: |
| 0-128 | TERMINAL, LUG; rd. tongue end; brass; tinned finish; $21 / 32 \mathrm{in} .1 \mathrm{lg} ., 3 / 8 \mathrm{in}$. wide, .020 in. thk; no. 10 stud; Zierick part no. 221-no, 10. | 3Z12073-44.40 <br> For replacement use SNSN G17-T-5114 |
| P-101 | CONNECTOR, PLUG; 1 round male contact; straight type; $31 / 32$ in. lg., $9 / 16$ in. dia.; cylindrical body, brass silver-plated, locking type; $1 / 4$ in. dia. max. cable opening; Waltham type UG-260 B/U. | $\begin{aligned} & \text { 2Z7390-260B } \\ & \text { N17-C-71408-9285 } \\ & \hline \end{aligned}$ |
| P-102 | CONNECTOR, PLUG; Same as P-101. |  |
| R-101 | RESISTOR, FIXED, COMPOSITION; 1.5 megohms $\pm 5 \% ; 1 / 2 \mathrm{~W}$ rated at 70 deg. C am bient temp.; .375 in .1 g ., 140 in . dia.; $1-1 / 2$ in lead length; insulated, resistant to humidity and salt-water-immersion; 2 wire lead terminals; Allen-Bradley part no. EB-1555. | 3RC20BF155J N16-R-51019-431 |
| R-102 | RESISTOR, FIXED, COMPOSITION; 150,000 ohms $\pm 5 f_{i \prime}^{\prime} ; 1 / 2 \mathrm{~W}$ rated at 70 deg . C ambient temp.; $.375 \mathrm{in} . \mathrm{lg} ., .140 \mathrm{in}$ dia., $1-1 / 2 \mathrm{in}$. lead length; insulated, resistant to humidity and salt-water-immersion; 2 wire lead terminals; Allen-Bradley part no. EB-1545. | 3RC20BF154J N16-R-50677-431 |
| R-103 | RESISTOR, FIXED, COMPOSITION; 15,000 ohms $\pm 5 \% ; 1 / 2 \mathrm{~W}$ rated at 70 deg. C ambient temp.; $.375 \mathrm{in} . \mathrm{lg} ., .140 \mathrm{in}$ dia., $1-1 / 2 \mathrm{in}$. lead length; insulated, resistant to humidity and salt-water-immersion; 2 wire lead terminals; Allen-Bradley part no. EB-1535. | 3RC20BF153J <br> N16-R-50335-43 |
| R-104 | RESISTOR, VARIABLE; composition; 2 sections; 1st section 2 megohms $\pm 20 \%$ second 3 solder lug terminals each section; metal inclosed case, $15 / 16 \mathrm{in}$. dia. $\times 1 \mathrm{in}$. deep; single rd. metal shaft $1 / 4 \mathrm{in}$. dia., $5 / 8 \mathrm{in}$. ig. from mtg. surface; normal torque; insulated contact dia., 32 thds/in., $1 / 4 \mathrm{in}$. $\lg$.; Mallory Dual type per Jet dwg. B-1184. | $\begin{aligned} & \text { 3Z7499-2.56 } \\ & \text { N16-R-89250-7579 } \end{aligned}$ |
| R-104A | Resistor, Variable. Part of R-104. | Listed for reference only. |
| R-104B | resistor, variable. Part of R-104. | Listed for reference only. |


| REF. <br> DESIG. | NAME OF PART AND DESCRIPTION | STOCK NOS. | SIG. CORPS STD. NAVY AIR CORPS | LOCATING FUNCTIONS |
| :---: | :---: | :---: | :---: | :---: |
| R-105 | RESISTOR, FIXED, COMPOSITION; 75 ohms $\pm 5 \% ; 1 / 2 \mathrm{~W}$ rated at 70 deg. C ambient temp.; 375 in . lg., 140 in . dia., $1-1^{\circ} 2 \mathrm{in}$. lead length; insulated; resistant to humidity and salt-water-immersion; 2 wire lead terminals; Allen-Bradley part no. EB-7505. | $\begin{aligned} & \text { 3RC20BF750J } \\ & \text { N16-R-49516-431 } \end{aligned}$ |  | Parasitic suppression pin 2 V -101A. |
| R-106 | RESISTOR, FIXED, COMPOSITION; 3.3 megohms $\pm 10 \% ; 1 / 2 \mathrm{~W}$ rated at 70 deg. C ambient temp.; $.375 \mathrm{in} .1 \mathrm{lg} ., 140 \mathrm{in}$. dia., $1-1 / 2 \mathrm{in}$. lead length; insulated; resistant to humidity and salt-water-immersion; 2 wire lead terminals; Allen-Bradley part no. EB-3351. | $\begin{aligned} & \text { 3RC20BF335K } \\ & \text { N16-R-51109-431 } \\ & \hline \end{aligned}$ |  | Grid return pin 2 V-101A. |
| R-107 | RESISTOR, FIXED, COMPOSITION; 3300 ohms $\pm 10 \% ; 1 / 2 \mathrm{~W}$ rated at 70 deg . C ambient salt-water-immersion; 2 wire lead terminals; Allen-Bradley part no. EB-3321. | $\begin{aligned} & \text { 3RC20BF332K } \\ & \text { N16-R-50066-811 } \end{aligned}$ |  | Cathode load resistor pin 3 of V-101A. |
| R-108 | RESISTOR, FIXED, COMPOSITION; $\mathbf{1 0 , 0 0 0}$ ohms $\pm 10 \%$; $1 / 2 \mathrm{~W}$ rated at 70 deg . C ambient temp.; $375 \mathrm{in} . \lg$., 140 in . dia., $1-1 / 2 \mathrm{in}$. lead length; insulated; resistant to humidity and salt-water-immersion; 2 wire lead terminals; Allen-Bradley part no. EB-1031. | $\begin{aligned} & \text { 3RC20BF103K } \\ & \text { N16-R-50281-431 } \\ & \hline \end{aligned}$ |  | Isolation resistor for internal sync signal. |
| R-109 | RESISTOR, FIXED, COMPOSITION; 10 megohms $\pm 10 \% ; 1 / 2 \mathrm{~W}$ rated at 70 deg . C ambient temp.; $375 \mathrm{in} . \lg$., 140 in . dia., $1-1 / 2 \mathrm{in}$. lead length; insulated; resistant to humidity and salt-water-immersion; 2 wire lead terminals; Allen-Bradley part no. EB-1061. | $\begin{aligned} & \text { 3RC20BF106K } \\ & \text { N16-R-51326-811 } \\ & \hline \end{aligned}$ |  | Isolation and voltage dropping resistor for cancellation of contact potential at R-104A. |
| R-110 | RESISTOR, FIXED, COMPOSITION; 100 ohms $\pm 5 \% ; 1 / 2 \mathrm{~W}$ rated at 70 deg. $C$ ambient temp.; $375 \mathrm{in} . \lg ., 140 \mathrm{in}$ dia., $1-1 / 2 \mathrm{in}$. lead length; insulated; resistant to humidity and salt-water-immersion; 2 wire lead terminals; Allen-Bradley part no. EB-1015. | $\begin{aligned} & \text { 3RC20BF101J } \\ & \text { N16-R-49579-431 } \\ & \hline \end{aligned}$ | $\cdots$ | Cathode bias resistor pin 3 of V-102. |
| R-111 | RESISTOR, VARIABLE; composition; 1 section, 500 ohms $\pm 20 \%$; $1 / 2 \mathrm{~W}$; 3 solder lug terminals, metal inclosed case $15 / 16 \mathrm{in}$. dia., 15/32 in. deep; single rd. metal shaft $1 / 4 \mathrm{in}$. dia., $5 / 8 \mathrm{in}$. lg. from mtg. surface; normal torgue; insulated; no "off" position; mtg. bush- ing $3 / 8-32,1 / 4$ in. $\lg$.; Allen-Bradley JAN type RV3ATRD501B. JAN spec R-94. | 3RV25028 <br> N16-R-87191-9330 |  | Adjustable cathode bias resistcr pin 8 of V-102. Vertical centering control. |


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| R－154 | RESISTOR，VARIABLE；composition； $1 \mathrm{sec}-$ tion， 500,000 ohms $\pm 20 \% ; 1 / 2 \mathrm{~W}$ ；one center tap； 4 solder lug terminals；inclosed metal case $15 / 16$ in．dia．$x 17 / 32$ in．deep；single rd． metal shaft $1 / 4$ in．dia．，5／8 in．lg．FMS；nor－ mal torque；insulated；no＂off＂position；mtg bushing $3 / 8 \mathrm{in}$. dia． 32 thd／in．， $1 / 4$ in．lg．， Mallory，per Jetronic dwg．no．B－1181． | $\begin{aligned} & \text { 3Z7498-50.202 } \\ & \text { N16-R-88181-8531 } \end{aligned}$ |
| :---: | :---: | :---: |
| R－155 | RESISTOR，FIXED，COMPOSITION； 2.2 me－ gohm $\pm 10^{\prime \prime} c ; 1 / 2 \mathrm{~W}$ rated at 70 deg． C ambient temp．；． $375 \mathrm{in} . \mathrm{lg} .$, ． 140 in ．dia．，1－1／2 in．lead length；insulated；resistant to humidity and salt－water－immersion； 2 wire lead terminals； Allen－Bridley part no．EB－2251． | 3RC20BF225K <br> N16－R－51065－811 |
| R－156 | RESISTOR，FIXED，COMPOSITION；Same as R－125． | －＊ |
| R－157 | RESISTOR，FIXED，COMPOSITION ；330，000 ohms $\pm 10 \% ; 1 / 2 W$ rated at 70 deg．$C$ ambient temp．； $375 \mathrm{in} . \lg ., .140 \mathrm{in}$ ．dia．，1－1／2 in．lead length；insulated；resistant to humidity and salt－water－immersion； 2 wire lead terminals： Allen－Bradley part no．EB－3341． | 3RC20BF334K <br> N16－R－50759－811 |
| R－158 | RESISTOR，VARIABLE；COMPOSITION； 2 sections； 1 megohm first section， 5 megohms rear section， $\pm 20 \%, 1 / 2 \mathrm{~W}$ both sections； 3 solder lug terminals each section；inclosed metal case $15 / 16 \mathrm{in}$ ．dia．， 1 in ．deep；single rd． metal shaft $1 / 4 \mathrm{in}$ ．dia．， $5 / 8 \mathrm{in}$ ．lg．FMS；nor－ mal torque；insulated；no＂off＂position：mtg bushing $3 / 8$ in．dia．， 32 thd／in．， $1 / 4$ in．lg．； Mallory Midgetrol type，per Jetronic dwg． B－1185． | $\begin{aligned} & \text { 3Z7499-5.23 } \\ & \text { N16-R-89232-1586 } \end{aligned}$ |
| R－158A | RESISTOR，VARIABLE，COMPOSITION； Part of R－158． | Listed for reference only |
| R－158B | RESISTOR，VARIABLE，COMPOSITION； Part of R－158． | Listed for reference only |
| R－159 | RESISTOR，FIXED，COMPOSITION ； 220 dhms $\pm 10 \% ; 1 / 2 \mathrm{~W}$ rated at 70 deg ． C ambient temp．； $375 \mathrm{in} .1 \mathrm{~g} ., .140 \mathrm{in}$ ．dia．，1－1／2 in．lead length；insulated；resistant to humidity and salt－water－immersion； 2 wire lead terminals； Allen－Bradley part no．EB－2211． | $\begin{aligned} & \text { 3RC20BF221K } \\ & \text { N16-R-49661-811 } \end{aligned}$ |
| R－160 | RESISTOR，FIXED，COMPOSITION；Same as R－149． | －． |
| R－161 | RESISTOR，FIXED，COMPOSITION ； 470 ahms $\pm 10 \% ; 1 / 2 \mathrm{~W}$ rated at 70 deg． C ambient temp．； $375 \mathrm{in} .1 \mathrm{~g} ., \mathrm{}$.140 in ．dia．，1－1／2 in．lead length；insulated；resistant to humidity and salt－water－immersion； 2 wire lead terminals； Allen－Bradley part no．EB－4711． | $\begin{aligned} & \text { 3RC20BF471K } \\ & \text { N16-R-49769-811 } \end{aligned}$ |


| $\begin{gathered} \text { REF. } \\ \text { DESIG. } \end{gathered}$ | NAME OF PART AND DESCRIPTION | STOCK NOS. <br> sig. CORPS <br> STD. NAVY <br> ANR CORPS | LOCATING FUNCTIONS |
| :---: | :---: | :---: | :---: |
| R-162 | RESISTOR, FIXED, COMPOSITION; Same as R -108. |  | Isolation for sync. grid pin 6 of V-108. |
| R-163 | RESISTOR, FIXED, COMPOSITION; Same as R -108. |  | Grid return pin 6 V-108. |
| R-164 | RESISTOR, FIXED, COMPOSITION; Same as R-151. |  | Grid return pin 7 V-105B. |
| R-165 | RESISTOR, FIXED, COMPOSITION; Same as R -108. |  | Plate load pin 6 V-105B. |
| R-166 | RESISTOR, FIXED, COMPOSITION; Same as R-161. |  | Cathode bias resistor pin 8 of V-105B. |
| R-167 | RESISTOR, FIXED, COMPOSITION; 22 ohms $\pm 10 \% ; 1 / 2 \mathrm{~W}$ rated at 70 deg. C ambient temp.; $375 \mathrm{in} .1 \mathrm{lg} ., .140 \mathrm{in}$. dia., $1-1 / 2 \mathrm{in}$. lead length; insulated; resistant to humidity and salt-water-immersion; 2 wire lead terminals; Allen-Bradley part no. EB-2201. | $\begin{aligned} & \text { 2RC20BF220K } \\ & \text { N16-R-49319-811 } \\ & \hline \end{aligned}$ | Surge suppression on input to CR-101. |
| R-168 | RESISTOR, FIXED, COMPOSITION; Same as R -167. |  | Surge suppression on input to CR-102. |
| R-169 | RESISTOR, FIXED, COMPOSITION; Same as R-137. |  | Filter resistor for high voltage power supply. |
| R-170 | RESISTOR, FIXED, COMPOSITION; 1000 ohms $\pm 10 \%$; 2 W rated at 70 deg. C ambient temp.; $688 \mathrm{in} . \lg ., ~ . ~ 312 \mathrm{in}$. dia., $1-1 / 2 \mathrm{in}$. lead length; insulated; resistant to humidity and salt-water-immersion; 2 wire lead terminals; Allen-Bradley part no. HB-1021. | 3RC41BF102K <br> For replacement use SNSN N16-R-49923- <br> 531 $\qquad$ | Filter resistor for low voltage power supply. |
| R-171 | RESISTOR, FIXED, COMPOSITION; Same as $\mathrm{R}-170$. |  | Filter resistor for intermediate voltage power supply. Horizontal amp. |
| R-172 | RESISTOR ,FIXED, COMPOSITION; 3300 ohms $\pm 10 \%$; 2 W rated at 70 deg. C ambient temp.; $.688 \mathrm{in} .1 \mathrm{lg} ., .312 \mathrm{in}$. dia., $1-1 / 2 \mathrm{in}$. lead length; insulated; resistant to humidity and salt-water-immersion; 2 wire lead terminals; Allen-Bradley part no. HB-3321. | 3RC41BF332K <br> For replacement use SNSN N16-R-50067501 $\qquad$ | Part of filter for intermediate voltage power supply. Vertical amp. In parallel with R-173. |
| R-173 | RESISTOR, FIXED, COMPOSITION; Same as R-172. |  | Part of filter for intermediate voltage power supply. Vertical amp. In parallel with R-172. |


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| $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \dot{\omega} \\ & \hline \end{aligned}$ | $\stackrel{\circ}{\square}$ | $\underset{\vec{H}}{\stackrel{\rightharpoonup}{3}}$ | $\begin{gathered} \stackrel{\rightharpoonup}{\partial} \\ \text { ஸ. } \end{gathered}$ | $\begin{aligned} & \text { ָ } \\ & \text { ஸ゙ } \end{aligned}$ | $\begin{aligned} & \text { 毋. } \\ & \text { ल゙ } \end{aligned}$ |  | $\begin{gathered} \text { 毋 } \\ \stackrel{\circ}{\mathrm{\omega}} \end{gathered}$ |



table 8-2. table of replaceable parts (Cont'd)

| $\begin{aligned} & \text { REF. } \\ & \text { DESIG. } \end{aligned}$ | NAME OF PART AND DESCRIPTION | STOCK NOS. $\begin{aligned} & \text { SIG. CORPS } \\ & \\ & \\ & \text { STD. NAVY } \\ & \text { AIR CORPS }\end{aligned}$ | LOCATING FUNCTIONS |
| :---: | :---: | :---: | :---: |
| X-105 | SOCKET, ELECTRON TUBE; Same as X-101. |  | Sceket for V-105. |
| X-106 | SOCKET, ELECTRON TUBE; Same as X-101. |  | Socket for V-106. |
| X-107 | SOCKET, ELECTRON TUBE; Same as X-103. |  | Socket for V-107. |
| X-108 | SOCKET, ELECTRON TUBE; 7 contacts, berryllium copper, silver-plated finish; miniature; $13 / 16$ in. dia., $1 / 2$ in. high incl. metal shock shield; center shield incl.; 1-3/32 in. lg., 13/16 in. dia., 29/32 in. high over-all, excluding terminals; low loss phenolic body; one piece saddle mtg., $5 / 8 \mathrm{in}$. dia. chassis hole required, 2 mtg . holes .125 in . dia. spaced 7/8 $\mathrm{in} . \mathrm{c}$ to c ; Eby part no. 9735-11. | 2Z8677.94 <br> For replacement use SNSN N16-S-626036702 $\qquad$ | Socket for V-108. |
| X-109 | SOCKET, ELECTRON TUBE; 12 contacts; spring brass, solder dipped finish; contacts no. 5 and 11 missing; miniature duo decal; 1-3/8 in . dia., $1 / 2 \mathrm{in}$. high over-all, excluding terminals; phenolic body; direct mtg. to contacts of cathode ray tube; Alden part no. 212MINC. | $\begin{aligned} & \text { 2Z8682.24 } \\ & \text { N16-S-64286-3985 } \end{aligned}$ | Socket for V-109. |
| X-110 | $\begin{aligned} & \text { SOCKET, ELECTRON TUBE; Same as } \\ & \text { X-108. } \end{aligned}$ |  | Socket for V-110. |

TABLE 8-3. MAINTENANCE PARTS KIT LIST

TABLE 8－4．CROSS REFERENCE PARTS LIST

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| 읓 |  <br>  <br> 〇゙ |
|  |  |
| 훈 | 멍్రం <br>  |
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| $\frac{6}{2}$ |  |  |  | E\% |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| 훛츤 |  |  |  |  |  |
|  |  <br>  <br>  ద్ల్ల M |  |  |  |  |
| 흘 |  <br>  | 흘 |  <br>  | Ale |  |
| $\begin{aligned} & 50 \\ & \frac{5}{2} \\ & \text { 2\% } \\ & \text { By } \end{aligned}$ |  |  |  |  |  |

## CAPACCITOR COLOR COOES




JAN E-DOT COLOR DODE FOR MMPER-DIELECTAIC CAPACITONS


RMA 0-DOT COLON COOE FOR MICA-DIELECTAK CAPACITORS
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CAPACITORS

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\begin{gathered}
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\hline 100
\end{gathered}
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\begin{aligned}
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& \text { SAN: SONNT ARMV- MAVY }
\end{aligned}
$$



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\end{array}
$$


TABLE 8-6. LIST OE MANUFACTURERS

\begin{tabular}{|c|c|c|c|}
\hline ABBREVIATION \& PREFIX \& NAME \& ADPRESS \\
\hline \begin{tabular}{l}
Aerovax \\
Allen-Bradley \\
Alden \\
Belden \\
Canfield \\
Centrolab \\
Cornell-Dubilier \\
Conant \\
Drake \\
Eby \\
Eleo \\
Fed. Telephone \& Radio \\
Garde \\
GE \\
Heyman \\
Ind. Trans. \\
Jetronic \\
Kurz-Kasch \\
Lord \\
Littlefuse \\
Mallory \\
Mueller \\
Oak \\
Precision Metal \\
RCA \\
Radio Receptor \\
Raytheon \\
Sprague \\
Waltham \\
Zierick
\end{tabular} \& CAW
CBZ
CYA
CQG
CBN
CD
CAZO
CAYS
CEB

CG
INTR
CBUA
CAUP
CAXP
CLF
CMA
CBIT
COC
CRC
CAFQ

CFS \& \begin{tabular}{l}
Aerovox Corporation <br>
Allen-Bradley Co. <br>
Alden Products Co. <br>
Belden Mfg. Co. <br>
Canfield Rubber Co. <br>
Centralab Division, Globe-Union <br>
Cornell-Dubilier Corp. <br>
Conant Electrical Labs <br>
Drake Mfg. Co. <br>
Hugh H. Eby <br>
Eleo Mfg. Co. <br>
Federal Telephone \& Radio <br>
Garde Mfg. Co. <br>
General Electric Co. <br>
Heyman Mfg. Ca. <br>
Industrial Transformer Corp. <br>
Jetronic Industries, Inc. <br>
Kurz-Kasch, Inc. <br>
Lord Mig. Co. <br>
Littlefuse, Inc. <br>
P. R. Mallory Co., Inc. <br>
Mueller Electric Co. <br>
Oak Mfg. Co. <br>
Precision Metal Products Co. <br>
Radio Corp. of America <br>
Radio Recepter Co., Inc. <br>
Raytheon Mfg. Co. <br>
Sprague Specialties Co. <br>
Waltham Horological Corp. <br>
Zierick MIg. Co.

 \& 

742 Belleville Ave., New Bedford, Mass. <br>
118 W. Greenfield Ave., Milwaukee, Wis. <br>
117 N. Main Street, Brockton, Mass. <br>
P. O. Box 5070A, Chicago, III. <br>
Bridgeport, Conn. <br>
900 E. Keefe Ave., Milwaukee, Wis. <br>
1000 Hamilton Blvd., Sa. Plainfield, N.J. <br>
6500 " 0 " Street. Lincoln. Nebraska <br>
1718 W. Hubbard St., Chicago, III. <br>
4700 Stenton Ave., Philadelphia, Pa. <br>
Philadelphia, Pa. <br>
East Newark, N.J. <br>
588 Eddy Street, Providence, R.I. <br>
1 River Road, Schenectady, N.Y. <br>
Kenilworth, N.J. <br>
Gouldsboro, Penna. <br>
Main and Cotton Sts., Phila., Pa. <br>
1421 So. Broaaway, Dayton, Ohio <br>
1639 W. 12th St., Erie, Pa. <br>
4765 Ravenswood Ave., Chicago, III. <br>
1941 Thomas St., Indianapolis, Ind. <br>
1597 E. 31st St., Cleveland, Ohio <br>
1200 N. Clybourne Ave., Chicago, Ill. <br>
Stoneham, Mass. <br>
Harrison, N.J. <br>
251 W. 19th St., New York, N.Y. <br>
Waltham, Mass. <br>
North Adams, Mass. <br>
Waltham, Mass. <br>
New Rochelle, N.Y.
\end{tabular} <br>

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\end{tabular}


[^0]:    * Data in this table apply to Oscilloscopes OS-8E/U manufactured by Carol Electronics Corp., 35 West Stephen street, Martinsburg, W. Va., under Contracts NObsr 75143 and 75682.

